Flow-net Relationships in the Forebay of John Day Dam

Annual Report 1982





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by Albert E. Giorgi

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ABSTRACT

During the spring of 1982, the National Marine Fisheries Service initiated a multiyear research program to define the effects of river conditions and dam operations on the current system (flow-net) in the forebay of John Day Dam on the Columbia River and to relate smolt passage behavior to the physical characteristics of the flow-net. Twelve digital, magnetic recording current meters were deployed in a grid within the restricted zone adjacent to the dam on 13 May 1982. Current velocity and direction were monitored until 3 November 1982. During this initial year, research efforts focused on gathering the first general data on flows within the forebay of John Day Dam and developing the computer software necessary to ultimately construct the flow-net model.

COALS AND OBJECTIVES

Even though collection and transportation facilities are operating at key dams in the Snake-Columbia Kiver System, significant numbers of juvenile salmonids continue to migrate downstream of their own volition (Sims et al. 1982). Improved fingerling bypass systems are being developed to ensure the safe passage of these migrants as they encounter the numerous dams on their seaward journey (McConnell and Muir 1982; Swan et al. 1982 and 1983).

Special flows, spills, and operating techniques at the dams are also being used to enhance smolt survival. These techniques are executed on the premise that the current system (flow-net) in each forebay responds to dam operations and that smolts in turn respond to the flow-net, as suggested by previous juvenile radio tracking studies conducted by the National Marine Fisheries Service (NMFS) in John Day forebay (Sims et al. 1981; Faurot et al. 1982).

The ultimate objective of the research program reported upon herein is to define the flow-net in the forebay of John Day Dam over a range of flow conditions and dam operations, and relate it to smolt passage behavior. Such information is fundamental in assessing the effectiveness of providing special flows and dam operations, and may also be useful in the design of fingerling bypass systems. To advance toward the ultimate objective, it is necessary to begin systematically gathering data and developing the cwputer software required to process and analyze the data. During 1982, we concentrated on these initial facets of the program.

METHODS AND MATERIALS

From 13 May to 3 November 1982, 12 self-contained, magnetic recording current meters (Interocean Systems, Inc., model 135 m 1 / were deployed in the forebay of John Day Dam. The meters were secured to a self-adjusting buoy system which maintained them at a constant depth, 3 m below the surface of the reservoir. Eleven of the meters were positioned in two parallel lines which spanned the length of the powerhouse and spillway approximately 115 and 365 m from the face of the dam (Figure 1). The 12th meter was stationed approximately 600 m from the dam and 100 m from the Oregon shore. Each hour both current velocity and direction were monitored for intervals ranging from 8 to 56 minutes. Cassette tapes and battery packs were replaced monthly to ensure that the meters continued to operate throughout the field season. Mechanical and electronic problems in these instruments did occur, thus the regular monthly inspections proved to be quite necessary.

Within the meter, data were recorded digitally on the magnetic tape cassettes in an 8-bit binary code. Current velocity was measured with a neutrally buoyant Savonius rotor mounted on carbide pivots running in jewel bearings. The operational range of velocities is rated as 5 to 300 cm.sec-1 \pm 1% of full scale reading. Direction was measured by a fluxgate magnetic compass over the full range of 0-359" \pm 3" magnetic.

Cassettes with encoded data were read into the Burroughs 7800 mainframe computer at the Northwest and Alaska Fisheries Center (NWAFC) via the digital cassette reader provided with the meters. The tape reader has minimal translating capabilities and merely transfers the coded data into

L/Reference to trade names does not imply endorsement by the National Marine Fisheries Service, NOAA.

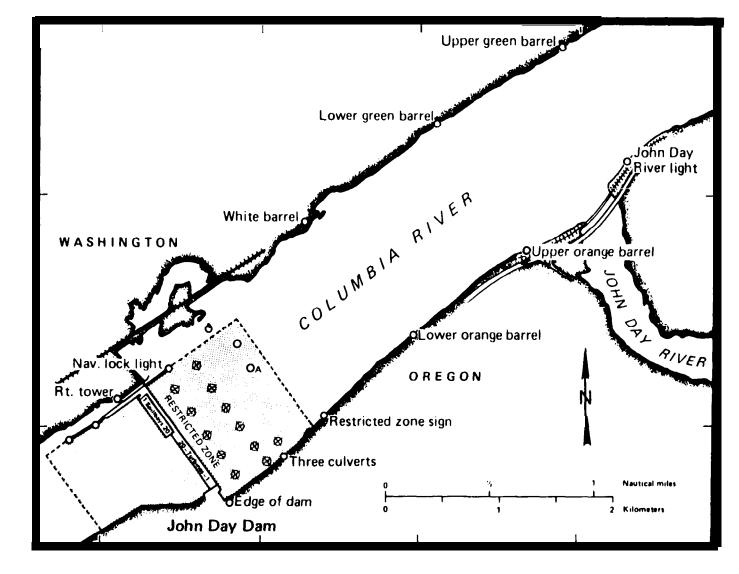


Figure 1.--Location of current meters (@) during the 1982 field season.

the mainframe. No software was provided by Lnteroceans Systems, Inc., thus the extensive and sophisticated programs necessary to process and analyze the data had to be developed by NMFS programmers in conjunction with the Biometrics Unit at the NWAFC.

The major components constituting the development of the flow-net model are outlined in Figure 2. Once the raw data was stored in the Burroughs 7800, the data must be checked for errors and edited before it is fit to be processed in the analysis program package. The data editing programs are still being developed; portions of the analysis program however, are operational at this time. Once we are satisfied with the performance of these programs, the current meter data will be meshed with the Columbia River Operational Hydronet and Management System (CROHMS) and dam operations data which are provided by the control room at John Day Dam, to produce the flow-net model. Some discrepancies between the CROHMS file maintained at the U.S. Army Corps of Engineers office in Portland, Oregon, and the control room data have been observed. Clearly, these conflicting data will affect the resolution of our model, and every attempt is being made to reconcile them. During 1982, in addition to gathering our initial set of data most of our efforts were directed at identifying and troubleshooting idiosyncrasies peculiar to this brand of current meter and developing the computer programs necessary to analyze the data.

RESULTS AND DISCUSSION

Inspection of data confirms that the current meters are effective in detecting changes in forebay currents (Figure 3). On 29 May 1982, with a river flow of 340 kcfs, current velocities increased from 20 to 35

JOHN DAY FLOW-NET STUDY

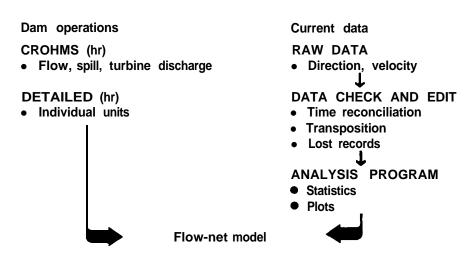


Figure L.--Flowchart summarizing the major components in the John Dal; Dan Flow-net Study.

POSITION 10

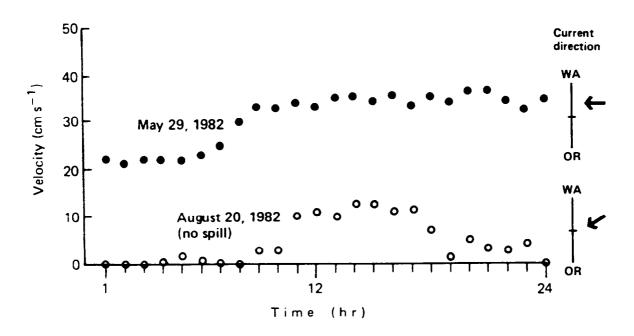


Figure 3.--Mean hourly current velocity at position 10 (center of spillway, 365 m from dam) on two different dates. For each day, the net current direction with respect to the dam (vertical line) is depicted to the right of the graph.

cm.sec-1 at position 10 (center of spillway, 365 m from the dam) as spill levels increased from 150 to 180 kcfs at 0700 h. Three months later, on 20 August, no spill was occurring and river flow had dropped to 205 kcfs. These conditions resulted in an overall decrease in current velocity from the 29 May levels and a concomitant shift in current direction away from the spillway towards the powerhouse. The increase in current velocity from 0 to approximately 12 cm.sec-1 on 20 August appears to be a consequence of increased power generation which typically occurs during the morning and continues through the evening hours.

Appendix A is an example of the intermediate, diagnostic data file, which details by hour, for a single location, the river conditions (total flow and turbine and spill discharge in kcfs and percent turbine and spill discharge) as well as the current velocity (cm.sec-1) and direction ("mag.). Inspection of these files allows us to assess current patterns at particular locations and detect any malfunctioning meters. Furthermore, and more importantly, these files form the foundation for constructing the flow-net model.

One of the major problems encountered during the first year's work was inherent to the manufacturers circuitry in the current meters. An independent data-time stamp was not provided with the serial current data, complicating and confounding necessary time reconciliation. To solve this problem, the NMFS' electronics shop developed a date-time stamp circuit to incorporate into the meter data. At the time of this report, the circuitry has been installed and successfully tested in 10 of the meters.

SUMMARY

- 1. Current patterns were monitioned within the restricted zone in John Day forebay from 13 May to 3 November 1982.
- 2. Current meter circuitry was redesigned by the NMFS electronics shop to provide date and time information with the serial data.
- 3. Portions of the computer software necessary to construct the flow-net model were developed.
- 4. During the 1982 field season we focused our attention on defining the flow-net near the dam. In 1983, we will attempt to determine how far upstream we can detect current fluctuations associated with dam operations and estimate the time lag involved between operation adjustments and current responses. We anticipate that by the end of 1983 a compllete computer programming package will be available for analyzing the John Day Dam flow-net. Additionally, we will track radio tagged juvenile chinook salmon in the forebay and evaluate their migratory behavior with respect to the prevailing current conditions.

SUMMARY OF EXPENEDITURES DURING 1982

Category:	Amount (\$ x 103):
Salaries	22.3
Transport	0.3
Travei	0.6
Contract Services	3.3
Supplies and Materials	4.2
Equipment	90.6 a/
Support	
(NOAA, DOC, S.L.U.C.)	10.1
	131.4

a/ Twelve current meters purchased from lnterocean Systems, Inc.

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APPENDIX A

Hourly river flows and current data for Meter 476 at Station Three, 29 September - 3 November 1982. The schematic display on the right side of each page depicts the current patterns for that hour. The lateral position of the asterisk relative to the heading at the top of the page (313, 213, 113°mag.) indicates the mean current direction for that hour. The center value (213°mag.) is normal to the face of the dam. The dashed arrow emanating from the asterisk represents the mean velocity at that meter (each printed character beyond the asterisk is equivalent to 2 cm.sec.-1).

DATE YR MGN CY	TIME SPAN	RIVER FLOW	TURBN FLOW	SPILL FLOW	HIVER	SPILL RIVER	DIRECTIO MEAN SD		CCITY N SD	313	213	
62 SEP 26	0 - 1	91.4	84.0	0.0	0.974	0.000						
	1 - 2	89. 5	86.7	0.0	C.953	0.000						
	2 - 3	90.2	£9.6	0.0	0.953	0.000						
	3 - 4	87.9	8/.3	0.0	C.993	0.000						
	4 - 5	91.6	91.0	0.0	C.793	0.000						
	5- €	74.6	94.0	0.0	0.994	0.000						
	6 - 7	110.3	107.9	0.0	0.978	0.000						
	3 - 6	111.0	110.4	0.0	C.995	0.000						
	8 - 5	116.3	115.7	0.9	0.955	0.000						
	9-10	128.1	127.5	0.0	0.995	0.000						
	10-11	129.5	127.1	0.0	0.981	0.000						
	11-12	129.4	126.6	n. u	0.995	0.000						
	12 -1 3 13 - 14	121.2 122.9	120.6	0.0 0.0	0.945	0.000 0.000						
	14-15	121.8	121.2	0.0	0.955	0.000						
	15-16	140.3	137.9	0. 0	0.983	0.000						
	16-17	139.2	136.6	0.0	0.956	0.000						
	17-18	132.3	131.7	0.0	0.955	0.000						
	18-19	130.8	130.2	0.0	0.795	0.000						
	19-20	132.1	131.5	0.0	0.955	0.000						
	20-21	123.4	122.6	0.0	0.995	0.000						
	222	115.3	114.7	0.0	0.995	0.000						
	25-53	104.4	103.E	0.0	0.954	0.000						
	23-24	100.0	97.6	0.0	0.976	0.000						
₹2 SEP 29	0 - 1	₹2 . 5	٤١٠۶	0.0	0.953	0.000						
	1 - 2	77.9	77.3	1. O	0.992	0.000						
	2 - 3	88.3	86.2	0.0	C. 353	0.000						
	3- 4	63.4	£2.£	0.0	0.953	0.000						
	4 - 5 5 - 6	83.1 00.8	82.5 88.2	0. 0 0. C	C.953 C.953	0.000						
	6 - 7	100.0	99.4	0.0	0.954	0.000						
	7 - 8	155.2	132.6	0. 0	C.955	0.000						
	8 - 9	122.7	122.1	0.0	C.995	0.000						
	7-10	128.8	126.2	0.0	0.955	0.000						
	10-11	127.3	126.7	0. 0	C.995	0.000						
	11-12	121.9	121.3	0.0	9.955	0.000						
	12-13	126.0	123.6	0.0	J. 961	0.000						
	15-14	123.1	122.5	C. 0	C.955	0.000						
	14-15	113.5	112.9	0.0	0.955	0.000	269 ••	0	0.0	1	:	
	1>-15	112.4	111.6	0.0	0.995	0.000	162 7			:	:	•->
	16-17	113.2	112.7	C. 0	C.9,6	0.000	158 7	4	0.7	:	:	* - >
	17 -18	121.9	121.4	0.0	0.996	0.000	157 6	7		:	•	* - • · >
	18-15	132.5	131.9	0.0	0.955	0.000	159 8	7	0.€	:	1	+>
	19-20	137.3	136.7	0.0	0.796	0.000	167 8	1.0		:	:	****>
	20 - 21	137.2	134.8	0.0	0.963	0.000	166 6	9		:	:	•>
	2: -22	127.3	124.9	c. 0	139.0	0.000	188 6	9		1	:	4 >
	22-23	122.7	122.1	0.0	0.955	0.000	188 6			:	1	****
	23-24	110.9	110.3	0.0	C.995	0.000	182 5	6	0.5	:	1	*>

GATE YR MON DY	TIME SPAN	PIVER FLOW	TURBN FLOW	SPILL FLOW	TUFER	SFILL RIVER	DIHFCT10 MEAN SD		0 C 1 T Y K S D	313	213	i i
62 SEP 30	0 - 1	87.8	85.4	0.0	C.9/3	0.000	169 6	3	0.3	:	t +->	:
	1 - 2	57.0	56.4	0.0	0.989	0.000	194 6		0.0	1	1 •	:
	2 - 3	52.0	51.4	C. 0	C.968	0.000	161 10	0	0.0	1	1 •	;
	3 - 4	51.9	51.3	0.0	0.586	0.003	175 14	0	0.0	•	: •	:
	4 - 5	51.8	51 • 2	C. O	0.988	0.000	171 11	C	C.C	1	1 •	:
	5 - (53.7	51.3	0.0	0.955	0.000	207 15		0.0	:	•	:
	6 - 7	81.5	79.1	0.0	0.9/1	0.000	183 12		9.0	1	:	:
	7 - E	143.1	142.5	0.0	C.996	0.000	183 7	7		:	: •••->	:
	8 - 5	135.3	134.7	0.0	0.956	0.000	172 7	6		:	: +==>	:
	9-10	127.1	1 26.5	0.0	0.995	0.000	162 12			:	t e->	:
	10-11	119.1	118.5	C. 0	C.995	0.000		TEST G		:	:	:
	11-12	128.6	126.0	9. 9	0.955	0.000	164 9	_		2	1 +->	:
	12-13	166.7	163.6	0.0	0.986	0.000	170 8	11		1	1 *****)	:
	13-14	139.0	137.4	n. o	0.996	0.000	170 6	-		•	****	:
	14 - 15	128.3	127.7	0.0	0.995	0.000	173 5	6	0.3	:	; +>	:
	15-16	117.1	114.7	0. 0	0.980	0.000	179 5			•	: •>	:
	16-17	114.1	113.5	0.0	0.955	0.000	162 7	4	1.0		1	•
	17 -18	114.4	113.t	V- 0	0.955	0.000	163 5	5		:	1 +->	:
	18 - 19	116.6	116.0	0.0	0.795	0.000	165 6			:	:>	:
	19-20	123.4	122.6	0.0	0.995	0.000	168 7	•		:	: •>	:
	20-21	118.3	117.7	7.0	0.995	0.000	170 7	6		:	: •>	•
	21 - 22	114.7	114.1	0.0	0.955	0.000	190 5	9		:	2 4>	:
	22 - 23	100.6	100.0	0.0	0.954	0.000	187 6			:	: •->	:
	23-24	98.7	98.1	0. 0	0.954	0.000	184 5	4	0.7	:	: •->	:
82 CCT 1	0 - 1	£ 4.2	61.E	0.0	0.971	0.000	180 4	4	0.6	:	: •->	•
	1 - 2	66.7	64.3	9. 0	0.964	0.000	177 7	Č		:	1	
	2 - 3	63.7	63.1	C. 0	C.991	0.000	179 8		0 • C	:	:	:
	3- 4	63.6	63.0	0.0	9.951	0.000	191 15	-	0.4	:	1 •	:
	4 - 5	65.4	64.8	0.0	0.991	0.000	187 13		0.3	:	: •	•
	5-6	€9.6	89.0	0.0	0.953	0.000	176 6	ž	0.9	1	• • • •	:
	6 - 7	113.4	112.6	0.0	0.995	U.000	179 9	6	1.1	:	: +>	
	7 - 8	126.2	125.6	C. 0	C.955	0.000	178 5	É	0.6	:	: 4>	:
	8 - 5	124.4	123.6	C. 0	0.255	0.000	161 6	e	0.7	:	: •>	
	9-10	140.E	120.6	0.0	0.995	0.000	178 9	6	3.0	:	1 4>	:
	10-11	120.8	120.2	0.0	C.995	0.000	185 4	7	0.7	:	: 4==>	:
	11-12	123.3	122.7	0.0	9.995	0.000	170 11	7	1.0	:	: •>	:
	12 - 13	126.7	126.1	0.0	C.995	0.000	165 10	6	0.9	:	: +>	:
	15-14	126. C	125.4	0.0	0.995	0.000	1/3 11	F	0.€	:	:	
	14-15	129.3	120.9	0.0	0.961	0.00	171 13	7	1.2	:	: ***>	1
	15-16	124.1	123.5	0.0	C.755	0.000	171 11	7	1.1	:	: *>	•
	16-17	125.3	124.7	0.0	C.995	0.000	155 12	€	1.C	:	1 +>	:
	17-18	151.7	131.1	0.0	0.955	0.000	164 10	9	0.9	:	t +>	:
	18-19	136.1	1 35.7	0.0	0.982	0.000	168 12	8	1.3	:	: •>	:
	19 - 20	137.5	136.5	0.0	0.356	0.000	161 9	ç	1.5	:	: ***->	:
	20-21	136.0	134.2	0.0	0.982	0.000	179 12	9	0.9	:	: •>	:
	21 - 22	11 3. C	112.4	0.0	(.755	0.000	185 7	9	C • 9	:	: •>	:
	55-53	106.1	105.5	0.0	0.954	0.000	166 9	7	1.1	:	: 4>	:
	23 - 24	€5.1	64.5	0.0	0.953	0.000	184 9	5	0.7	:	1 +>	1

DATE YR MON CY	I IME SPAN	RIVER FLOW	TUREN FLOW	SPILL FLD#	IUFEA FIVER	SPILL RIVER	DIRFCTIUN MEAN SC			31 3	213	11
e2 CCT 2	0 - 1	£0.1	77.7	٥. ٥	U.970	0.000	186 17	6	2.1	:	: *>	:
	1 - 2	76.6	70.0	0.0	0.952	0.000	201 14	2	1.0	:	: •>	:
	2 - 3	77.1	76.5	C. 0	C.942	0.000	202 12	1	0.6	:	•	:
	5 - 4	81. t	61.2	U. 0	0.953	0.000	182 7	3	1.0	1	; •>	:
	4 - 5	83.3	82.7	0.0	C.993	0.000	198 7	4	0.€	1	: •->	:
	5 - €	€5.7	85.1	0.0	0.993	0.000	205 12	3	0.5	1	: **>	:
	6 - 7	£ 2.9	82.3	0.0	0.953	0.000	197 12	4	0.€	:	: ••>	:
	7 - E	96.3	95.7	0.0	0.954	0.000	197 7	4	1 . C	:	1 4->	:
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	y -1 C	111.2	110.6	0.0	C.955	0.000	195 €	€	0.7	:	; +=->	:
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	11-12	109.5	106.9	0.0	0.955	0.000	164 9	7	0.7	:	: +>	:
	12-11	100.9	100.3	0.0	C. 954	0.000	192 10	E	C • 7	2	: •••>	:
	13-14	19.0	96.4	n. D	0.954	0.000	186 6	E	0 . E	:	: +>	:
	14-15	98.3	97.7	0. U	0.994	0.000	188 11	7	1 . C	:	: •>	:
	15-16	97.3	36.7	C. 0	0.954	0.000	178 13	7	0.9	:	: •••>	:
	16-17	95.3	94.7	0.0	0.954	טייָט . ט	167 13	6	1 - 1	:	: •>	:
	17-16	y5. /	95.1	0.0	0.954	0.000	182 9	6	0.6	1	; •>	:
	18-19	106.8	104.4	0.0	0.578	0.000	184 10	7	1.0	:	: •>	:
	19-20	lut.b	106.0	0.0	0.994	0.000	189 7	8	0.9	:	: +>	:
	20-21	105.3	104.7	C. 0	0.954	0.000	191 9	8	C.7	:	1 +>	:
	21 - 22	99.3	9t.7	0.0	0.994	0.700	2110 9	7	0.7	:	: ****>	:
	22 - 23	98.2	97.6	0.0	0.994	U.U00	199 12	€	0.7	:	: +>	:
	25-24	87.9	87.3	0.0	0.993	0.000	195 10	6	0.7	1	1 4**>	:
62 CC1 3	0 - 1	76.3	73.5	0.0	0.969	0.000	201 5	6	1.3	2	: +>	:
	1 - 2	74.0	73.4	0. 0	0.957	0.000	193 8	3	0.7	:	; +->	:
	2 - 3	10.6	7 C . C	0.0	0.952	0.000	195 7	2	0.5	:	: •>	:
	3 - 4	10.2	69.6	0.0	0.951	0.000	184 11	4	9.0	:	t +->	:
	4 - 5	64.4	63.8	0.0	0.9>1	0.000	189 9	3	1.0	2	: ••>	:
	5 - 6	63.5	€2.9	0.0	0.951	0.000	168 10	1	0.E	:	1 +>	:
	5 - 7	62.9	62.5	0.0	0.950	4.000	165 9	1	1.1	:	1 +>	:
	7 - 8	14.1	73.5	0.0	C. 792	0.000	175 9	2	1.2	:	: •>	:
	6- 5	75.0	74.4	0.0	0.952	0.000	163 10	2	0.9	:	: •>	:
	9-10	75.1	74.5	0.0	0.992	0.000	179 11	2	1.1	2	;	:
	10-11	76.4	75.8	C. 0	0.9>2	0.000	162 13	1	0.9	:	: *>	:
	11-12	76.6	70.0	V. U	0.992	0.000	189 11	1	0.6	1	: •>	:
	12-13	80.7	7 t. 3	0.0	C.97C	0.000	197 8	3	0.5	:	: 4->	:
	13-14	78.8	7 E . 2	ე. ა	0.997	0.000	185 4	1	0.9	:	: •>	:
	14-15	75.3	75.7	0.0	C.952	0.000	191 4	1	0.4	:	: +>	:
	15 -1€	17.5	75.1	C. 0	€.9€9	0.000	187 5	1	0.€	:	: •>	:
	16-17	€ Q. O	75.4	9.0	0.953	0.000	187 5	2	0.6	*	; •>	:
	17-18	82.4	80.0	0.0	0.971	0.000	182 €	2	0.7	:	: +>	:
	18 - 1 9	87.6	81.C	0.0	C.953	0.000	183 7	2	9.0	:	: *>	:
	17-20	33. €	93.2	0.0	0.994	0.000	166 6	4	0.7	:	: +->	:
	20-21	92. A	92.2	0.0	C.994	0.000	175 9	4	0.7	:	: +->	:
	21 - 22	8. 0	87.4	0.0	0.993	0.000	175 12	3	0.7	:	: ••>	:
	22 - 23	97 . 1	96.5	0.0	0.954	0.000	169 9	5	0.6	2	: ••>	:
	23-24	101.2	100.6	0. 0	0.954	0.000	175 9	5	C.7	:	: •->	:

DATE YR PON CY	T 1 M F S P A R	FLOW FIVER	TURBN Flow	SPILL FLOW	IUEEN Fiver	SPILL	DIHEC MEAN	TION SD	V E L L L M E A N		313	213	11'
£2 OCT 4	o - 1	81.1	78.7	0.0	0.970	0.000	185	11	3	1.0	ı	1 *>	:
	1 - 2	17.3	76.7	C. C	C.752	0.000	194	7	5	0.9	3	1 •>	:
	2 - 3	69.6	69 .0	n. n	0.951	0.000	191	11	1	1.0	1	: •>	:
	5 - 4	10.9	70.3	o. o	0.352	0.000	177	e	Ç	0.2	1	! •	:
	4 - 5	12.6	12.0	C. O	C.972	0.000	189	7	1	0.7	1	1 •	:
	5- €	£3.2	3.09	ი. ა	0.971	0.000	192	11	2	0.9		: *>	:
	6-7	102.7	102.1	0. 0	0.954	0.000	174	7	3	1 - 1	:	1 **>	:
	7 - 8	108.3	107.7	0.0	0.954	0.000	177	10	4	1.0	1	* *->	:
	8 - 9	107.0	105.4	0.0	0.954	0.000	169	7	4	0.6	:	1 4*>	:
	9-10	103.0	102.4	0.0	C.954	0.000	169	8	5	0.6 0.6	:	• • • •	-
	10 - 11	96.5	55.5	0.0	0.994	0.000	177	6	4		:	• • • • • •	:
	11 - 12	99.0	99.0	0.0	0.594	0.000	173	9 u	4	0. £	:	: •-•>	:
	12 -1 3	100.2	99.6	C. 0	0.754	0.000	175	6	6	0.5	•	•-•>	•
	13-14	100.8	100.2	0.0	0.954	0.000	172		5	0.7	:	. ,	:
	14-15	9 P . 2	37.6	0.0	0.954	0.000 0.000	184 180	7 E	5	6.€	•	•••>	:
	15 - 16	37.1	96.5	C. 0	0.994	0.000	175	9	6	0.7		1 •••>	:
	16-17	105.6	105.0	0.0 0.0	0.994	0.000	171	11	6	0.8	i	**->	:
	17-18	107.6	107.0		0.75	0.000	171	15		0.6	1	1>	•
	16-15	113.9	113.3	0.0	0.995	0.000	170	7	ź	0.7			•
	19 - 20	126.6	126.0	0.0 0.0	0.916	0.000	176	13	6	1.0	:	•••)	:
	20 - 21	99.8	97.4 98.4	0.0	0.754	0.000	167	lâ	6	0.5		: +>	:
	21 - 22	99.0		0.0	0.976	0.000	177	7	5	0. €	:	1 •••>	:
	22 - 2 3 23 - 24	101.2	98.8 97.2	0.0	0.954	0.000	174	ż	5	0. t	:	; +->	:
	63-64						-		_				:
£2 CC1 5	0 - 1	99.0	98.4	ი. 0	0.554	0.000	177	6	6	0.6	:	: +->	:
	1 - 2	98.3	27.7	0. 0	C.994	0.000	188	7	5	C. E	:	: +->	:
	2 - 3	74.1	93.5	7.0	0.954	0.000	166	7	4	9.0	:		:
	3 - 4	95.9	92.3	0.0	0.994	0.000	180	5	4	1.2	:	:	:
	4 - 5	94.1	93.5	0. 0	0.994	0.000	179	4	4	0.6	:	• • • •	:
	5 - €	96.2	93.8	0.0	C. 975	0.000	163	4	•	1.0	:	•••>	•
	6 - 7	119.7	119.1	0.0	0.995	0.000	163	ť	7	1.1	•	••••>	:
	7 - 8	126.2	125.6	0.0	0.995	0.000	186	6	8 7	0.E	:	: •>	:
	6 - 5	117.6	117.2	0.0	0.955	0.000	191	8	4	0.6	•	>	:
	9-10	94.1	93.5	0.0	0.994	0.000 0.000	187 184	ę	10	1.0	:		:
	10-11	111.0	110.4	0.0	0.995	0.000	164	9	10	0.9	:	>	:
	11 - 12	109.7	109.1	0.0	C.977	0.000	184	9	10	1.3	•	1 ()	:
	12-13	103.1	100.7	0. 0 n. n	0.977	0.000	191	12	11	1.2	•	1 4)	:
	15-14	10 3 . 3 99 . 4	100.9 98.8	0.0	0.994	0.000	191	• 9	13	1.6	•	>	:
	14-15	97.7	91.1	C. 0	0.994	0.000	187	á	10	2.1	•	>	:
	15 - 1 6 16 - 17	96.2	95.6	0.0	0.994	0.000	176	18	9	1.6	1	; ,•••>	:
	17-18	102.1	101.5	0. 0	0.954	0.000	166	18	í	1.3	:	; ,)	:
	18-15	114.2	113.6	0.0	C.955	0.000	153	ii	1 C	0.7	:	; ,>	:
	19-20	139.3	129.7	0.0	0.995	0.00)	177	10	11	1.0	:	: ****>	:
	20 - 21	128.7	128.1	0.0	C.955	0.000	175	6	ii	0.e	:	:>	:
	21 - 22	125.2	124.6	7.0	C. 155	0.000	171	9	10	0.6	:	:	:
	22 - 23	112.6	112.0	0.0	0.955	0.000	164	11	8	1.3	:	: +>	:
	23-24	105.3	104.7	C. 0	C.994	0.000	159	7	7	0.6	:	: •>	:

DATE YR PON DY	I IME S PAR	FLOW	TUF BN FLOW	SPILL FLOW	PIAL H	SPILL RIVER	DIHEC		VELC		313	213		1 1
£2 0CT 6	0 - 1	97.2	96.6	0.0	0.754	0.000	160	7	5	0. t	:	:	**~ >	
	1 - 2	95.4	94.8	0.0	C.954	0.000	150	7	5	0.5	:	:	4->	
	2 - 3	94.4	95.6	0.0	0.954	0.000	153	6	5	0.6	:	:	·>	
	3 - 4	96. 3	93.9	C. 0	C.915	0.000	159	7	5	C • 2	:	:	**>	
	4 • 5	95.2	94.6	0.0	0.994	0.000	172	P	•	0.7	:	1	•••>	
	5 - 6	96.1)	95.4	0.0	0.954	0.000	177	7	5	0.6	:	:	•>	
	6 - 7	103.0	100.6	0.0	0.977	0.000	173	7	6	0.4	:	.	** - >	•
	1 • E	125.1	124.5	0.0	0.995	0.000	174	ē	ę	0.4	:		*>	
	£ = 9	125.1	124.5	0.0	0.995	U.0 (n)	161	7	8	0.€	:	:	*>	
	y-10	125.1	124.5	0.0	0.755	0.000	159	12	?	0.7	:	1	* >	
	10-11	125.6	125.0	0.0	0.955	0.000	172	7	ę	0.6	•	:	•>	
	11-12	124.6	124.C	0.0	0.755	0.000	147	8	9	0.€	:	i	•>	•
	12-13 13-14	126.4	124.C	0.0	0.981	0.000	140	12	9	1.2		•	*=>	
		124.8	124.2	0.0	0.355	0.000	149	10	£	1.4	•		+ >	
	14-15 15-16	126.1	125.5	0.0	0.955	0.000	152	10	9	1.1	•	1	4***)	:
	16-17	126.6 130.4	124.2	0.0 0.0	0.981 0.995	0.000	149	, E	£ g	1.1	1	•	••••	
	17-18	133.4	129.6	0. 0	0.995	0.000	147		9	1.3	i	•	•	
	16-15	146.4	132.E 144.0	0.0	0.984	0.000 0.000	164	10 10	10	C. E 1.2	:	•	4>	
	19-20	146.9	145.4	0.0	0.756	0.000	158	13	9	1.1	•	•	*****	
	20-21		145.7	0.0	C.9E4	0.000	155					•	•••••)	
	21-22	148.1 129.2	124.6	0.0	0.95	0.000	145	10 15	7 C	1.2	•	•	4>	
	22-23	116.3	114.9	0.0	0.988	0.000	159	12	7	1.6 1.2	:	•	****	,
	23-24	108.7	108.1	0.0	0.994	0.000	169	9	ż	0.5	•	•	4**>	
	63-64	100.7	1001	0.0	0.,,,	0.0.0	103	•	•	0.,	•	•	,	
£2 OCT 7	0 - 1	103.4	102.E	0.0	0.954	0.000	172	10	5	1.0	:	:	•->	
	1 - 2	100.5	99.5	0.0	C.994	0.000	154	15	4	0.9	1	:	•->	
	2 - !	99.7	99.1	0.0	0.994	0.000	150	9	5	0.9	:	.	••>	
	3-4	99.4	96.E	0.0	0.994	0.000	151	11	5	0.9	:	1	•>	
	4 - 5	98.3	97.7	0.0	C. 994	0.000	152	11	6	9.0	:	1	•>	
	5• €	98.7	96.1	0.0	0.954	0.000	157	9	6	0.7	1	1	*>	
	6 - 7	104.6	104.0	0.0	0.954	0.000	149	10	5	1.C	:	1	*->	
) - E	125.3	124.7	C. 0	C.355	0.000	155	9	5	0.9	:	1	•>	
	e - 5	126.6	12t.2	0.0	0.955	0.000	154	12	7	0.6	1	:	>	:
	9-10	134.4	133.8	0.0	0.796	0.000	148	1 i	e	1.3	:	.	4>	:
	10-11	134.5	133.7	0.0	0.996	0.000	155	14	9	1.3	2	:	*****	:
	11 - 1 8	134.4	135.€	0.0	0.956	0.000	159	13	9	1.1	1	z	•>	-
	12 - 1 3	134.4	133.6	C. O	0.956	0.000	156	9	7	1.1	:	1	+>	
	13-14	154.4	133.6	0. n	0.956	0.00	157	15	ŧ	1 - 1	:	:	* >	
	14-15	134.4	133.6	0.0	11.956	0.000	154	10	8	1.1	:	1	*>	
	15-16	132.5	131.5	C. 0	C.755	0.000	147	9	9	1 . C	2	:	•>	
	16-17	126.0	125.4	0.0	0.995	0.000	149	14	ė	1.4	1	:	*>	:
	17 - 18	130.0	129.4	0. 0	0.955	0.000	146	13	e	1.2	:	1	4>	;
	16-19	137.6	137.C	C. 0	C.996	0.000	154	11	9	1.0	:	:	****>	
	19 - 20	141.2	140.6	1.0	0.956	0.000	155	11	9	1.5	:	:	•>	
	20 - 21	141.2	138.8	0.0	0.963	0.000	151	10	8	1.1	:	:	4>	
	21 - 22	129.7	120.6	0.0	0.955	0.000	166	11	٤	1.0	:	.	()	:
	22 - 23	109.3	106.7	0.0 0.0	C.995 C.975	0.000	166	10	€ ,	1.1	:	:	••• >	
	23-24	15.7	93.3	V. V	(• 7 f J	0.000	155	11	4	1.1	•	ī	+->	·

DATE YR PON CY	T IME S P A R	RI VER FLOW	TURBN FLOW	SPILL FLOW	IUEEN FIVFR	SPILL RIVER	DIKEC MFAN	110N SD	VELCO MEAR		315	213		1:
£2 0CT 8	0 - 1	93.5	92.9	0.0	0.994	0.000	156	13	1	0.9		<u>:</u>	•>	
	1 - 2	93.1	92.5	0.0	C . 994	0.000	160	13		1.0	1	1	*>	
	2 - 3	91.5	91).9	0.0	0.953	0.000	149	7	3	1.0		•	4*>	
	3- 4	90.)	90.3	0. 0	0.953	0.000	149	9	4	1 • C	:	•		
	4- 5	21.3	90.7	7.0	0.953	0.000	155	ē	3	0.3	:	•	4>	•
	5 - 6	106.9	106.3	0.0	0.954	0.000	163	9	6	0.3	:	•	•••>	
	6- 7	112.6	11C.2	0.0	0.979	0.000	177	6	Ę	0.5	•	•	*>	
	7 - E	122.4	121.6	0.0	0.955	0.000	179	5	7	0.5	•	•	4===)	;
	8 - 5	125.2	124.6	0. 0	(.995	0.000	179	6	ę	0.6	•	•	* >	:
	y -10	128.7	126.1	0.0	0.935	0.000	160	5	£ 9	0.4 U.E	:	•	•=•->	:
	10-11	133.6	133.0	J. U	0.996	0.000	179	5 5	9	0.5	:	· ·	*****	:
	11-12	134.5	1 33.7	0.0	C.956	0.000	179	5	9	0.4		•	•>	:
	12-13	136.1	135.7	0.0	C.962	0.030	178 174	5	9	1.7	:	:	•>	:
	13-14	135.4	135.0	0.0	0.962	0.000	179	6	9	0.2	:	•	•>	:
	14-15	133.6	135.0	0.0	0.996 0.996	0.000 9.000	164	3	9	0.0			>	:
	15-1€	133.6	133.0	0.0	0.956	0.000	176	7	9	0.3	;	:	*>	:
	16-17	140.8	140.2	0.0			-	, 6	10	0.6	•	:	*****	:
	17 -1 6	140.7	14C-1	C. O	0.996	0.000	181 189	6	10	0.4	:	:	>	:
	16-15	143.0	142.4	0.0	0.956		184	7	1 C	0.5		•	* >	
	19-20	144.6	142.4	0.0	0.983	0.000	178	6	9	1.7	:		•===>	•
	20 - 21	137.8	131.2	0.0	0.956 0.956	0.000	161	5	10	1.7	:	1	*>	:
	21 - 55	136.7	136.1	0.0	0.955	0.000	183	í	ě	0.6		3	*>	:
	22 - 23	126.4	125.8	0.0 0.0	0.954	0.000	160	5	ě	0.4		1	***>	•
	23 - 24	99.9	99.3	v. v	4. 774	0.000	100	,		•••	•			
	۸- ۱	76.9	76.3	0. 0	0.952	0.000	174	6	2	0.6	:	:	+>	:
FS 0C1 9	0 - 1	86.9	P4.5	0. 0	C. 912	0.000	158	8	3	C.5	:	:	+ - >	:
	2- 3	£2.7	£2.1	0.0	0.953	0.000	150	9	ă	0.7	:	:	• - >	
	3-4	t 2.9	82.3	0.0	C.953	0.000	157	7	3	0.5	:	1	•->	:
	4-5	82.1	81.5	0.0	0.993	0.000	160	7	3	0.7	:	1	** >	•
	5 - €	e 3. o	82.4	0.0	0.953	0.000	162	7	4	0.4	:	:	* +>	•
	6-7	93.1	92.5	0. 0	C.954	0.000	167	7	5	0.6	:	1	+->	
	7 - 8	109.0	106.4	0.0	0.954	0.000	164	7	E	0.6	:	:	•>	
	£ = 9	130.0	129.4	0.0	0.955	0.000	173	9	1 C	1.1	:	:	*>	:
	9-1C	142.0	141.4	0.0	C.996	0.000	112	9	1 C	9.0	:	1	*>	:
	10-11	142.0	141.4	0.0	0.996	0.000	175	e	9	0.5	:	:	*>	3
	11-12	159.5	136.9	0.0	0.983	0.000	170	9	9	3.0	:	1	*>	:
	12 - 13	128.0	125.6	C. 0	C.961	0.000	112	8	10	1 . C	:	:	4>	:
	15-14	117.7	117.1	0.0	0.755	0.000	179	9	10	1.0	:	:	•>	:
	14-15	110.7	110.1	0. 0	0.295	0.000	189	6	8	0.€	:	:	•>	:
	15-16	106.7	106.1	0.0	C.954	0.000	186	8	7	0.9	:	1	•>	:
	16 - 17	105.1	104.5	0.0	0.954	0.000	160	9	e	1.2	:	:	•>	:
	17 - 18	110.0	109.4	0. 0	C.955	0.000	183	12	8	0.7	:	:	*>	:
	18-19	122.4	121.8	0.0	0.755	0.000	185	10	9	0.7	:	:	• • • • >	:
	19-20	124.7	124.1	0.0	0.995	0.000	177	6	9	3.0	:	:	•>	:
	20-21	110.5	109.9	C. O	C.9;5	0.000	117	7	8	0.9	:	:	• • • • >	:
	21 - 22	110.2	109.6	0.0	0.955	0.000	174	7	e	2.1	:	•	4>	:
	22-23	111.8	111.2	U. 0	0.935	0.000	175	6	7	9.0	1	•	 >	;
	23-24	100.9	10C.3	C. 0	C.954	0.000	169	7	E	0.4	:	1	+>	•

DATE YR MUN CY	TIME	HI VER FLOW	TURBN FLOW	SPILL FLUW	IUBEN Fiver	SPILL	DIREC MEAN		VELC ME A N		313	213	1	
82 OCT 10	0 - 1	89.1	84.5	0.0	0.993	0.000	157	7	5	0.5	:	:	+ >	
	! • 2	77.5	76.9	0.0	0.952	0.000	155	7	4	0.3	:	:	« - >	
	2 - 3	77.6	75.4	n. 1)	C. 969	U . O 10	147	13	7	1.2	:	1	+)	
	3 - 4	17.4	76.8	G. 0	0.952	0.000	144	8	4	1.C	:	:	•->	
	4- 5	9.09	80.2	0.0	0.993	0.000	166	ŧ	4	0.7	:	:	•->	-
	5 - E	£5.6	62.0	0.0	0.993	0.000	156	7	4	0.5	:	:	•->	•
	6 - 7	90.9	90.3	0.0	0.993	0.000	163	8	4	0.7	:	:	+->	
	1- 8	99.8	99.2	0.0	0.994	0.000	160	10	5	0.7	:	:	*->	•
	8 - 9	94.6	92.4	0. 0	0.915	0.000	161	8	4	0.6	:	:	+->	
	9-1C	94.3	93.7	0.0	0.954	0.000	143	9	3	0 · E	1	:	• - >	•
	10-11	100.0	97.6	ე. ს	0.9/6	0.000	137	9	7	1.0	:	1	4>	:
	11-12	93.3	92.7	C. 0	C. 994	0.000	132	6	5	0.€	:	:	411.00	
	12 • 1 !	95.7	93.3	0.0	0.975	0.000	124	10	5	1.0	:	1	* ~~ >	:
	13-14	94.1	93.5	0.0	0.994	0.000	140	9	6	1.2	:	:	•>	•
	14 - 15	71.0	90.4	C. 0	0.953	0.000	137	5	7	1.C	:	:	* >	
	15-16	91.6	89.2	n. 0	0.974	0.070	177	9	E	0.7	1	:	*>	:
	16-17	92.1	91.5	0.0	0.993	0.000	171	8	7	9.0	:	:	•>	:
	17 - 16	88.7	1.83	0.0	0.993	0.000	158	11	5	0.7	:	:	*>	:
	16-15	95.4	94.6	0.0	0.994	0.000	161	11	4	1.0	:	:	*->	:
	19-20	117.8	117.2	0. 0	0.955	0.000	161	9	8	1.0	:	1	*>	:
	20 - 21	100.5	98.2	C. 0	C.716	0.000	157	9	5	0.6	:	:	•>	:
	21 - 22	67.1	66.5	0.0	0.993	0.000	142	4	5	0.8	:	:	*~ >	:
	22 - 23	91.5	89.1	0. 0	0.974	0.000	142	7	5	0.8	:	:	+ >	:
	23-24	108.5	107.9	0.0	0.954	0.000	154	7	7	0.6	:	:	•>	:
£2 CC 1 11	0 - 1	t1.6	81.0	0.0	0.993	0.000	146	6	5	0.€	:	:	***)	:
	1 - 2	64.7	84.5	C. 0	0.793	0.000	139	6	5	C.5	:	:	• >	:
	2 - 2	£5.4	₽2.9	0.0	0.971	0.000	139	5	5	0.4	:	1	+- >	:
	3 - 4	83.1	82.5	o. o	0.993	0.000	143	5	5	0.4	1	:	a->	:
	4 - 5	85.7	85.2	0.0	0.934	0.000	143	E	4	0.6	1	:	*=>	:
	5 - E	6 . 6	8£.2	0.0	0.993	0.000	141	6	4	0.e	:	1	+->	:
	6 - 7	121.1	120.5	c. o	C.955	0.000	154	6	8	0.6	:	:	•>	:
	7 - E	126.9	126.3	n. 0	0.955	0.000	168	۴		0.€	:	:	4>	:
	6 - 9	126.3	125.7	0.0	0.955	0.000	164	e	7	0.6	:	:	·>	:
	9-10	138.4	137.8	C. O	C.996	0.000	156	11	9	1.0	:	:	A>	:
	10 - 11	156.9	156.3	9.0	0.996	0.000	150	9	10	0.6	:	:	•>	:
	11-12	156.9	156.3	0. 0	0.996	0.000	156	10	9	1.C	:	:	• >	:
	12 - 13	135.2	134.6	0.0	C.996	0.000	149	9	7	0. t	:	:	* >	:
	13-14	131.5	130.6	9. 0	0.995	0.000	14€	£	ŧ	0.6	:	I	* >	:
	14-15	142.0	141.4	0.0	0.996	0.000	144	7	9	1.8	:	:	•>	:
	15-16	142.5	141.9	0.0	0.956	0.000	155	9	9	0 • £		•	h>	ĭ
	16-17	126.4	124.0	0.0	0.981	0.000	152	11	7	1.4	:	£	*>	:
	17-18	133.6	133.C	0. C	C.996	0.000	148	8	9	0.7	2	:		:
	10-15	131.1	130.7	0.0	0.955	0.000	153	е	9	0.5	:	1	>	:
	19-20	138.7	138.1	0.0	0.996	0.000	171	9	e	0.€	:	1	·>	:
	20-21	134.3	133.7	C. 0	C.956	0.000	176	6	8	0.E	:	:	• >	:
	21 - 22	122.2	121.6	0.0	0.995	0.000	176	5	7	0.4	:	:	•>	:
	22 - 23	118.4	116.0	C. 0	0.980	0.000	180	5	7	C.5		1	***>	:
	23-24	110.5	109.9	0.0	0.455	0.000	169	5	€	0.€	:	2	4>	:

DATE YR MUN CY	TIME SPAN	RI VER FLOW	TURBN FLOW	SPILL FLUH	IURAN RIVER	SPILL	DIREC MEAN	TICN SD	VEL C		313	213		1:
na 00 t 12	0 - 1	108.7	106.3	C. 0	C.978	0.000	164	7	6	C. 5	:	1	•>	
82 OCT 12	1 - 2	106.1	105.5	ñ. 0	0.994	0.000	164	7	5	0.7	:	2	*>	
	2-3	110.6	108.2	J. 0	0.978	U.000	146	5	6	0.7	3	1	4 >	
	3- 4	109.4	106.8	0.0	0.955	0.000	170	8	5	C. 7		ı	* >	
	4	110.6	110.0	0.0	0.755	0.000	157	5	7	0.7	1	1	• >	:
	5-6	104.8	102.4	0.0	0.917	0.C00	150	7	7	1.0	1	1	*>	:
	6- 7	123.2	122.6	0.0	C. 795	0.000	152	7	9	0.7	:	1	•>	:
	7- 8	121.2	120.6	0.0	0.255	0.000	145	6	7	0.7	2	3	*>	:
	8 - 5	123.0	120.6	0.0	0.980	0.000	149	8	7	1.0	1	1	4>	•
	y-10	117.6	112.0	C. 0	0.995	0.000	149	9	5	0.7	1	I	• - >	:
	10-11	116.8	116.2	0.0	0.995	0.000	156	9	6	0.5		1	·>	:
	11-12	133.3	1 32.7	0.0	0.995	0.000	1 48	10	6	0.6	t .	1	4~~>	:
	12-13	133.3	132.7	0.0	0.955	0.000	146	5	€	0.6	1	1	•>	:
	13-14	126.4	125.8	0.0	0.995	0.000	154	10	7	9.0	3	1	•>	•
	14 - 15	126.4	125.8	0.0	C.995	0.000	151	7	8	C • 9	:	1	****)	
	15-16	121.4	119.0	0.0	0.960	J. 000	143	e	7	0.8	•	1	•==->	
	16-17	119.6	119.2	0.0	C.955	0.000	143	9	7	0.7	:	1	••••>	•
	17-16	132.6	137.0	0.0	0.955	0.000	161	7	10	3.0	:		*****	_
	16-15	129.2	126.6	0.0	0.995	0.000	172	9	Ę	1.1	:	•	4-4->	•
	19-20	131.C	175.6	0.0	C.962	0.000	164	8	8	0.6	•	1	****	
	20 - 21	127.3	126.7	ი. 0	0.995	0.000	166	6	6	0.5	:	1	•>	
	21 - 22	119.1	116.5	0.0	0.955	0.000	170	6	7	9.0	:	1	*>	:
	55-53	117.8	117.2	0.0	0.995	0.000	162	8	7	C. E	:	:		•
	23-24	96. €	96.2	0.0	0.954	0.000	157	5	5	0.7	:	1	*>	·
62 CCT 13	0 - 1	102.1	101.5	0.0	C.994	0.000	165	8	4	0.E	:	ı	e->	•
	1 - 2	100.8	100.2	C. 0	C.994	0.000	149	5	5	0.4	:	.	4 >	:
	2- 3	101.3	100.7	0.0	0.954	0.000	157	7	6	0.5	:	•	* >	•
	3 - 4	104.6	104.0	0.0	C.994	0.000	148	5	6	C. 3	:	1	•>	:
	4 = 5	112.2	109.6	9.0	0.979	0.000	155	7	E	0.7	1	1	***>	•
	5 - 6	122.6	122.0	ე. ი	0.995	0.000	154	8	7	0.9	:	.	•>	
	6 - 7	135.5	134.9	0.0	0.996	0.000	151	6	8	0.6	:	: -	•>	:
	7 - 8	143.3	142.7	0.0	0.956	0.000	167	10	10	0.7	:	•	• • • • · · · ·	:
	6 - 9	156.6	156.2	0.0	0.985	0.000	177	8	11	0.7	:	1	,>	:
	9-1C	141.2	138.8	0.0	0.983	0.000	184	7	9	0.0	:	:		:
	10-11	145.8	145.2	0.0	0.956	0.000	153	10	9	1.0		•	4-0->	
	11 -12	144.9	144.2	0.0	0.996	0.000	171	9	٩	0.7		•	*****	
	12 • 1 3	145.0	144.4	0.0	0.956	0.000	156	Ę	8	0.6	:	•	¢)	:
	13-14	144.8	144.4	0.0	0.997	0.000	152	7	10	0.7	•	•	*****	:
	14-15	144.7	144.1	0. 0	C.956	0.000	158	9	11	0.6	•	•		:
	15-16	140.4	139.0	0.0	0.956	0.000	176	9	12	0.9	:	•	*****	:
	16 - 17	130.2	129.6	0.0	0.995	0.000	170	11		1.0	•	•		:
	17 -16	115.3	114.7	0.0	C.955 O.919	0.000	168	11 13	8	0.8	:	•	****	:
	16-15	116.6	114.4	0.0		0.000	167 175	10	7	0.9	:	•	****>	:
	19-20	117.5	114.9	0.0	0.9E0	0.000	171	12	έ	1.1	•	•	•>	:
	20 • 21	117.4	115.C	0.0 0.0	0.955	0.000	183	9	7	0.5	•	•	·>	:
	21 - 22	115.5	114.9 113.5	0.0	0.995	0.000	155	'n	7	0.6	:	- 2	* >	÷
	22 • 2 3 23 • 2 4	114.1 94.6	52.2	0.0	0.975	0.000	170	5	,	0.7	i	-	4>	1
	63-64	7 4 4 0	76.06	V1.7	4.,,,	3.000	1.0	•	•	•••	-	•		

DATE YR MON DY	TIME SPAR	RI VER FLOW	IURBN Flow	SPILL FLUW	IUREN FIVER	SPILL RIVER	DIRECTION MEAN SO	VELC:		31 3	213	11
62 CCT 14	0 - 1	95.7	95.1	0.0	C.994	0.000	160 6	5	0.4	:	1 *->	:
	1 - 2	99.7	99.1	0.0	0.954	0.000	170 7	6	U.5	:	↓ •••>	:
	2 - 3	101.1	100.5	0.0	0.994	0.000	155 5	6	0.0	:	1 ***>	:
	3 - 4	102.6	102.C	0.0	0.954	0.000	161 7	5	0.€	1	: +==>	3
	4- 5	101.1	100.5	0.0	0.994	0.000	163 /	6	0.2	1	1 •>	:
	5 - 6	109.8	109.2	0.0	0.995	0.000	166 /	6	0.5	1	1 4>	:
	6 - 7	125.4	124.8	0.0	0.995	0.000	157 7	6	0.6	:	1 +>	
	7 - 8	147.6	145.2	0.0	0.984	0.000	157 7	8	0.5		t +>	I .
	6- 9	147. d	147.2	0.0	0.996	0.000	154 8	9	0.5	t	:	
	3-10	144.8	144.2	0.0	0.956	0.000	164 E 17E 7	10	0.5	:	:	
	13-11	150.6	150.2	0.0	0.996	0.000	- -	10	0.6	:	: •>	•
	11-12	150.8 150.8	150.2 150.2	0.0	0.996 0. 996	0.000 0.000	175 6 178 6	10 10	0.6 0.4	:	;	•
	12-13	148.7	140.3	0.0	0.984	0.000	157 9	9	0.7	•	: *****	•
	13-14 14-15	145.6	145.0	0.0	0.996	0.000	152 9	1 C	0.6	:		•
	15-16	147.0	140.4	0.0	0.996	0.000	149 8	11	0.4	•	1 4	·> :
	16-17	146.2	145.6	0.0	C.956	0.000	157 7	9	0.6	•	1 ****>	•
	17 - 18	146.2	145.6	0.0	0.996	0.000	171 10	11	1.0	· •	1 (******)	:
	16-19	147.9	147.3	0.0	0.996	U.000	169 E	10	0.6	1	1>	:
	19-20	148.0	147.4	C. 0	0.996	0.000	163 10	9	1.7	:	: ••••>	1
	20-21	150.3	147.5	0.0	0.964	0.000	173 10	10	0.6	:	: 4>	:
	21-22	144.6	144.2	0.0	0.996	0.000	168 10	ç	0.7	:	: +>	:
	22 - 23	147.6	145.2	C. 0	6.984	0.000	173 9	9	0.6	:	: 4>	:
	23-24	116.6	116.0	0.0	C.995	0.000	165 9	6	0.9	2	1 ****>	:
62 OCT 15	0 - 1	102.0	101.4	0. 0	C.954	0.000	165 7	6	0.5	1	: •>	:
02 001 13	1 - 2	112.3	111.7	ç. ö	0.995	0.000	153 6	ě	0.4	:	i •>	:
	2-3	108.1	107.5	0.0	0.994	0.000	150 5	6	0.7	1	1 *>	:
	3 - 4	89.5	86.9	0.0	0.993	0.000	148 6	4	0.5	:	: 4->	:
	4 - 5	91.1	50.5	0.0	0.993	0.000	154 6	4	0.7	1	: +->	:
	5 - 6	108.3	195.9	v. 0	0.978	0.00 0	155 7	5	0.6		: +=>	:
	6 - 7	1 51.0	136.4	C. C	0.995	0.000	153 8	7	0.6	:	: 4**>	:
	7 - E	141.6	141.0	0.0	0.996	0.000	154 8	9	0.9	1	: 4>	:
	£ - 9	141.6	141.0	0.0	0.996	0.000	154 9	9	0.9	ı	1 4)	:
	y-10	143.5	142.9	0.0	0.996	0.000	154 12	9	1.2	:	: ****>	:
	10-11	140.7	140.1	0.0	0. 996	0.000	161 10	9	0.9	:	: ****>	:
	11-12	140.7	140.1	0. 0	0.956	0.000	160 8	10	0.7	1	: 4>	:
	12 - 13	145.5	144.9	0.0	0.756	0.000	156 8	1 C	0.7	:	: •>	•
	13-14	156.1	155.5	n. n	11.996	0.000	160 9	9	3.0	:	: •>	:
	14-15	160.2	157.6	0.0	C.985	0.000	160 9	9	C.7	:	: •••••	I .
	15-16	154.0	153.4	0.0	0.956	0.000	159 9	10	1.0		1 4>	
	16-17	153.3	152.7	0.0	0.956	0.000	167 10	1 0	1.7	:	; ,>	:
	17 - 16	167.2	164.8	0.0	0.986	0.000 0.000	162 9 160 11	11	1.2	:	1 4>	•
	10-15 19-20	167.2	166.6	4).0 C.0	0.956	0.000	158 11	10 10	0.8	:	:	•
	20-21	166.6 155.0	166.0	0.0	0.956	3.000	155 10	9	1.2	•	:	
	21 - 22	148.4	147.8	0.0	0.996	U.000	158 9	ģ	1.2	:	1 + + + + + + + + + + + + + + + + + + +	:
	22-23	136.3	135.7	0.0	0.956	0.000	159 11	í	0.9	:	: +>	:
	23-24	116.4	116.0	0.0	0.960	0.000	149 12	É	0.7	2	: +>	:
				,	J.,.J	· · · ·	• • • • •	•		-	• •	- -

AH KAN CA OVIE	TIME SPAN	RIVER FLOW	TURBN FLOR	SPILL FLUW	APANT APATA	STILL FIVER	DIRECTION MEAN SD	V & L C :		31 3	21 3		1 .
82 CC I 16	0-1	11 9. 5	117.1	0.0	0.780	0.000	145 8	6	0.7	:	1	4>	
00 001 10	ĭ - ?	104.7	104.1	0.0	0.954	0.000	15é 9	4	0.5	:	:	•->	
	2- 3	ye. 3	97.1	0.0	C. 994	0.000	155 6	3	0 . E	:	1	•->	
	3 - 4	95. t	94.5	0.0	0.994	0.000	151 7	4	0.5	:	:	••>	
	4-5	98. t	96.2	0.0	0.954	0.0 00	161 11	5	0.6	:	:	*>	
	5-6	97.5	96.9	0.0	0.994	0.000	156 7	5	0.5	t	1	>	
	6- 7	96.1	95.5	0.0	0.954	0.000	165 14	5	1.0	1	:	**>	
	/- b	97.5	96.9	n . 0	0.994	0.000	159 11	5	1.0	:	:	*>	
	8 - 9	107.7	107.1	0.0	0.954	0.000	169 11	6	3.0	:	:	>	
	9-10	121.9	121.3	n. a	0.955	0.000	166 12	7	0.7	:	:	*>	-
	10-11	123.5	1 22. 9	0.0	C. 995	0.000	156 10	E	0.8	:	:	*>	:
	11-12	123.2	122.6	0.0	0.95	0.000	156 10	7	0.€	:	3	•>	:
	12-13	122.9	122.3	0.0	0.995	0.000	161 13	ę	1.0	:	2	*~~~ >	:
	13-14	122.2	121.6	0.0	0.955	0.000	153 11	7	1.3	1	:	•>	•
	14 - 15	112.1	111.5	0.0	0.955	0.000	161 12	7	1.0	:	:	*>	:
	15-16	112.6	110.2	v. v	0.979	U.000	162 13	6	0 . e	:	1	•>	:
	16-17	120.9	118.5	0.0	0.960	0.000	172 11	7	3.0	:	:	*>	:
	17 - 16	121.0	120.4	0.0	0.955	0.000	168 11	ŧ	0.9	1	•	• >	•
	16-19	129.5	1 26.9	0.0	C. 995	0.000	179 8	9	1.1	:	ı	*>	•
	19 - 20	137.8	1 37 . 2	0.0	C.996	0.000	166 17	9	C. 9	1	•	* >	:
	20 - 21	133. 1	132.5	0.0	0.995	0.000	184 11	ę	1.0	:	:	* >	_
	21 - 22	133.8	1 31 . 4	0.0	0.982	0.000	182 6	e	C.7	:		*>	
	22 - 23	122.7	122.1	0.0	0.955	0.000	177 10	8	1.3	:	•	•>	
	25-24	118.3	117.7	0.0	0.995	0.000	175 11	ŧ	1.0	:	•	*>	•
82 CCT 17	0 - 1	115.6	115.0	0.0	C. 195	0.000	160 17	7	1.3	:	:	*>	
	1 - 2	100.5	55.9	0.0	0.994	0.000	172 13	ŧ	1.1	:		+>	
	2 - 3	97 . 6	97.2	0.0	0.994	0.000	175 13	7	1.0	:	:	*>	
	3- 4	97.2	96.6	0.0	C.994	0.000	142 8	7	0.6	:		•>	
	4- 5	98.2	97.6	n. n	0.994	0.000	183 8	7	1.0	1	2	·>	•
	5-6	100.3	99.7	0 . 0	0.994	0.000	190 9	€	0.7		:	•>	
	6 - 7	102.2	99.8	0.0	0.977	0.000	178 10	7	3.0	1		+>	
	7 - E	100.0	99.4	0.0	0.954	0.000	177 9	5	1.0	:	:	+->	
	8 - 9	105.1	104.5	0. 0	0.994	0.000	191 9	6	0.7	ı	:	•>	
	9-1C	132.0	131.4	0.0	0.995	0.000	177 13	9	0 • E	:	1	•>	
	10-11	132.6	132.2	0.0	0.995	0.000	180 12		0.9	:	•	•>	•
	11-12	131.2	1 30.6	0.0	C.955	0.000	185 8	8	0.7	:	•	****>	:
	12-1!	130.9	130.3	0.0	0.955	0.000	186 8	e	1.2	:	1	•>	•
	13-14	129.3	126.7	0.0	0.955	0.000	182 10	8	0.9	:	1	**** <u>*</u>	,
	14-15	131.2	126.8	0.0	C.982	0.000	184 8	8	C.7	•	1	• • • • >	
	15-16	129.5	128.9	0.0	0.955	0.000	167 7	9	0.9	:	•	****	:
	16-17	127.3	128.7	0.0	0.995	0.000	183 7	1 C	1.4	:	<u>.</u>	*>	,
	17 - 1 8 16 - 15	130.9	130.3	0. 0 0. 0	C.955 Q.955	0.000 U.000	189 6 164 /	9 9	1.3	:	: :	****>	:
	14-20	133.0	1 32.4	0. 0	C.955	0.000	196 8	9	1.1	:		4000	
	20-21	135.1	132.7	0.0	0.962	0.000	163 8	9	0.8	•	•	****>	
	21-22	133.0	132.4	0.0	0.955	0.000	167 6	ě	0.7	•	•	*>	
	22 - 23	132.3	131.7	C. 0	C.955	0.000	191 8	9	0.9	•	•	****>	:
	23-24	127.9	127.3	0.0	0.955		193 8	9	0.6	:	•	*>	:

82 CCT 18	DATE YR PUN DY	I IME SPAR	RI VER Flow	TURBA FLOW	SPILL FLOW	IUSEN FIVER	SPILL	DIREC MEAN	TIGN SD	VELC MEAN		31 3	21	3	1
2-1	82 CCT 18			113.3	0. C	0.955	0.000	189	7	e	0.5	:	:	*>	
3		_					0.000	198	10	€	0.5	:		+>	
*** **** **** **** **** **** **** **** ****				89.4	0.0	0.993	0.000	189	6	6	0.€	2	1	· · · >	
5 - 6 114.7 118.1 0.0 C.953 0.000 187 4 7 0.7 : : :				92.9	c. o		0.000	1 + 3	6	5	0.6	1	:	* >	
0 - 7 161.4 159.0 0.0 0.245 0.000 177 7 10 0.7 1 1 1 1 1 1 1 1 1			_				0.000	189	٤	5	0.6	:		+~->	
7 - 2 184.5 189.2 0.0 0.997 0.000 179 13 1.2 1 1.2 1 1.2 1 1.2 1 1.2 1 1.2 1 1.2 1 1.2 1 1.2 1.2 1 1.2 1.2 1 1.2								187	4	7	0.7	:	:	+>	
						_			7	10	0.7	:	:	*>	
								179		13	1.2	:	1	*>	
10-11 105.0 164.4 0.0 0.956 0.000 101 7 12 0.5 1 1 1 1 1 1 1 1 1					0.0			191	10	14	1.C	:	:	•>	
11-12 1 4.7.9 144.9 0.0 0.945 0.000 1 127 5 1 C 0.4 1							0.000	165		13	0.7	:	:	*>	
12-12			165.0	164.4	0.0	0.996	0.000	181	7	12	0.5	:	:	*>	
13-14					0.0		0.000	187	5	1 C	0.4	:	:	•>	
14-15									8	12	0.6	:	:	·>	
15-16 14-8.2 147.6 0.0 0.956 0.000 188 8 1.1 1.2 1.0 1 1.1					C. O	0.996	0.000	190	7	11	C • 6	1	:	*>	
16-17					0.9		0.000	192	10	11	9.0	:	:	 >	
12-16 14-9, 3 14-7 0.0 0.956 0.000 177 0 12 1.0 1 1.5 1.5			148.2	147.6		0.996	0.000	192	11	12	1.0	:	:	•>	
16-19 155.3 154.7 0.0 0.956 0.000 165 0.10 170 0 0 170 0 0 170 0 0 170 0 0 170 0 0 170 0 0 170 0 0 170 0 0 170 0 0 0 170 0 0 0 0 0 0 0 0 0							0.000	188	8	12	1.1	:	:	•••••>	
17-26				146.7	0.0	0.996	0.000	177	ç	12	1.0	:	:	*~~~>	:
20-21 154.7 154.1 0.0 0.956 0.000 167 11 12 1.2 1 1.2 1.2 1.2 1 1.2		16-19	155.3	154.7	0.0	0.956	0.000	165	8	11	1.5	:		*>	
21-22 154.b 154.0 0.0 0.956 0.000 158 12 13 1.2 :		-	1 > 5.8	155.2	0.0	C.956	0.000	170	9	12	0.6	:	t	*****	
22-21 153.8 153.2 0.0 C.96 0.000 158 12 13 1.3 : :				-	0.0	0.956	0.000	161	11	12	1.2	:	:	*>	
23-24 152.4 151.6 0.0 0.956 0.000 166 9 12 1.3 :				154.0	0.0	0.996	0.000	169		13	1.2	:	:	******	
82 OCT 19			153.8	153.2	0.0	C.956	0.000	158	12	13	1.3	:	:	*)	>
1 - 2		23-24	152.4	151.6	0.0	0.956	0.000	166	9	12	1.5	1	1	*****	
2- 3	82 OCT 19	0 - 1	153.9	151.5	0.0	0.984	0.000	161	10	12	1.0	:	:	*	
3- 4 157.7 137.3 0.0 0.996 0.000 162 10 9 0.7 :		1 - 2		131.4	0.0	0.956	0.000	177	e	11	1.0	:	:	*****	
4-5 149.2 148.6 0.0 0.956 0.000 160 10 9 0.4 1		2 - 3	134.7	134.1	0.0	0.956	0.000	164	9	10	0.9	:	:	* >	
5-6 157.7 157.1 0.0 0.996 0.000 158 6 9 1.7 : :		-		-	0. 0	0.996	0.000	162	10	9	0.7	:	1	*>	
6-7 187.3 186.6 C.C 0.996 0.000 169 7 13 1.1 : : :		•		148.6	0.0	0.956	0.000	160	10	9	0.4	1	:	*>	
7 - E 309.5 20E.5 0.0 0.957 0.000 173 10 16 0.9 1		5- 6	157.7	157.1	0.0	0.996	0.000	158	6	9	1.7		:	*>	
d= 5		6 - 7	-	186.6	C.C	0.996	0.000	169	7	13	1.1	:	:	*****	
9-1C 162.4 161.8 0.0 0.956 0.000 180 7 11 0.6 : 10-11 154.3 151.9 0.0 0.964 0.000 174 5 8 0.4 : 11-12 145.6 145.0 0.0 0.996 0.000 175 5 11 0.3 : 12-12 147.2 146.6 0.0 0.996 0.000 189 8 10 0.4 : 13-14 139.3 136.7 0.0 0.996 0.000 179 9 11 1.1 : 14-15 137.4 136.8 0.0 0.996 0.000 182 6 11 1.0 : 15-16 140.4 135.8 0.0 0.996 0.000 182 6 11 1.0 : 15-17 168.0 167.4 0.0 0.996 0.000 188 11 15 1.2 : 17-16 17 0.7 170.1 0.0 0.996 0.000 187 9 14 1.4 : 11-15 171.2 170.7 0.0 0.996 0.000 187 9 14 1.4 : 11-16 17 17.3 170.7 0.0 0.996 0.000 187 9 14 1.4 : 11-17 168.0 168.0 169.4 0.0 0.996 0.000 187 9 14 1.4 : 11-18 171.2 170.7 0.0 0.996 0.000 187 9 14 1.4 : 11-19 171.2 170.7 0.0 0.996 0.000 177 7 11 0.7 : 11-20 168.6 168.0 0.0 0.0 0.996 0.000 180 7 10 0.9 : 11-22 167.9 167.5 0.0 0.996 0.000 187 7 11 0.7 : 11-22 167.9 167.5 0.0 0.996 0.000 187 7 11 0.7 : 11-22 167.9 167.5 0.0 0.996 0.000 165 8 9 0.5 :		} - €	209.5	20E.5	0.0	0.757	0.000	173	19	16	U.9		:	*>	
10-11 154.8 151.9 0.0 0.984 0.000 174 5 8 0.4 : : :> 11-12 145.6 145.0 0.0 0.996 0.000 175 5 11 0.3 : :> 12-13 147.2 146.6 0.0 0.996 0.000 169 8 10 0.4 : : :> 13-14 139.5 138.7 0.0 0.996 0.000 179 9 11 1.1 : : :> 14-15 137.4 136.8 0.C C.996 0.000 182 6 11 1.C : : :> 15-16 140.4 133.6 0.0 0.996 0.000 188 11 1.5 1.2 : :> 16-17 168.0 167.4 0.0 0.996 0.000 188 11 15 1.2 : :> 17-16 17 0.7 170.1 0.0 0.996 0.000 187 9 14 1.4 : :> 11-20 168.6 16d.2 0.0 0.996 0.000 187 5 10 13 0.8 : :> 20-21 168.6 16d.2 0.0 0.996 0.000 180 7 10 0.9 : :> 21-22 167.9 167.5 0.0 0.996 0.000 180 7 10 0.9 : :> 22-23 123.5 152.5 0.0 0.996 0.000 165 8 9 0.5 : :>				194.1	0.0	C.997	0.000	168	10	1.4	0.5	:	:	>	
11-12 145.6 145.0 0.0 C.996 0.000 175 5 11 0.3 :		9 - 1 C	162.4	161.8	0.0	0.996	0.000	180	7	11	0 . E	:	3	*>	
12-13 147.2 146.6 0.0 0.956 0.000 169 8 10 0.4 : :			154.5	151.9	9.9	0.964	0.000	174	5	8	0.4	:	*	*>	
13-14 139.3 13£.7 0.0 0.996 0.000 179 9 11 1.1 : :			145.6	145.0	0.0	C.996	0.000	175	5	11	0.3	:	:	A>	
14-15 137.4 136.8 0. C C.956 0.000 182 6 11 1. C : :> 15-16 140.4 135.6 0. 0 0.956 0.000 193 9 12 0.7 : :> 16-17 168.0 167.4 0. 0 0.956 0.000 188 11 15 1.2 : :> 17-18 17 0.7 170.1 0. 0 0.956 0.000 187 9 14 1.4 : :> 16-15 171.3 170.7 0. 0 0.956 0.000 185 10 13 0.8 : :> 17-20 168.6 16d.2 0. 0 0.956 0.000 177 5 11 1.3 : :> 20-21 168.6 168.0 0. C 0.956 0.000 180 7 10 0.5 : :> 21-22 167.9 167.3 0. 0 0.956 0.000 187 7 11 0.7 : :> 22-23 103.5 152.5 0. 0 0.956 0.000 165 8 9 0.5 : :>				146.6	0.0	0.956	0.000	169	8	10	0.4	:	*	>	
15-16 140.4 135.6 0.0 0.956 0.000 193 9 12 0.7 : 16-17 168.0 167.4 0.0 0.956 0.000 188 11 15 1.2 : 17-16 17 0.7 170.1 0.0 0.996 0.000 187 9 14 1.4 : 16-15 171.3 170.7 0.0 0.956 0.000 185 10 13 0.8 : 17-20 168.6 168.2 0.0 0.956 0.000 179 5 11 1.3 : 20-21 168.6 168.0 0.0 0.996 0.000 180 7 10 0.9 : 21-22 167.9 167.3 0.0 0.996 0.000 187 7 11 0.7 : 22-23 103.5 152.5 0.0 0.996 0.000 165 8 9 0.5 :		15-14	139.5	136.7	0.0	0.996	0.000	179	9	11	1.1	2	:	4>	
16-17 168.0 167.4 0.0 0.956 0.000 188 11 15 1.2 : :			137.4	136.8	0. C	C.996	0.000	162	6	11	1.C	:	:	* >	
17-18 17 0.7 170.1 0.0 0.996 0.000 187 9 14 1.4 : :> 16-15 171.3 170.7 0.0 0.996 0.000 185 10 13 0.8 : :> 17-20 168.6 168.2 0.0 0.996 0.000 179 5 11 1.3 : :> 20-21 168.6 168.0 0.0 0.996 0.000 180 7 10 0.9 : :> 21-22 167.9 167.3 0.0 0.996 0.000 187 7 11 0.7 : :> 22-23 1>3.5 152.9 0.0 0.996 0.000 165 8 9 0.5 : :>		15-1€	140.4	139.6	0.0	0.995	0.000	193	9	12	0.7	:	:	>	:
16-15 171.3 170.7 0.0 0.956 0.000 185 10 13 0.8 :		16-17	168.0	167.4	0.0	0.956	0.000	188	11	15	1.2	2	:	*>	•
17-20 168.6 16d.2 0.0 0.996 0.000 179 5 11 1.3 : :> 20-21 168.6 168.0 0.0 0.996 0.000 160 7 10 0.9 : :> 21-22 167.9 167.3 0.0 0.996 0.000 167 7 11 0.7 : :> 22-23 1>3.5 152.9 0.0 0.996 0.000 165 8 9 0.5 : :>					0.0	C.996	0.000	187	9	14	1.4	:	:	*****	•
20-21 168.6 168.0 0.C C.996 0.000 160 7 10 0.5 : :				170.7	0.0	0.956	0.000	185	10	13	0.8	:	:	•>	
21-22 167.9 167.3 0.0 0.996 0.000 177 7 11 0.7 : :> 22-23 1>3.5 152.5 0.0 0.996 0.000 165 8 9 0.5 : :>		-		160.2	0.0		0.000	179	5	11	1.3	:	:	*****	
22-23 1>3.5 152.5 0.0 0.996 0.000 165 8 9 0.5 :					0. C		0.000			1.0	0.5	:	:	*>	
			167.9	167.3	0.0	0.996	0.000	177	7	1 1	0.7	:	:	>	
23-24 147.7 147.1 0.0 0.996 0.000 178 7 8 0.4 : :>					C. 0			165	e	9	0.5		:	•>	
		23-24	147.7	147.1	0.0	0.996	0.000	178	7	£	0.4	:	:	·>	

DATE YR PUN CY	T IME Span	RIVER FLOW	TUHBN FLOW	SPILL FLUH	IUPEN BIVER	SPILL FIVER	DINEC MEAN	T I U N S D	VELC MEAN		313	213	1
82 CCT 20	0 - 1	139.9	1 39.3	0.0	0.796	0.000	157	Ŋ	ę	0.7	:	:	• = = >
02 55, 25	1 - 2	128.3	127.7	0.0	0.955	0.000	145	5	7	0.5	1	1	•>
	2 - 3	126.5	125.9	n. 0	0.995	0.000	147	1 t	7	1.1	1	1	*>
	3 - 4	129.5	128.9	0.0	C.995	0.000	157	11	7	1 • 1	:	:	+>
	4- 5	124.6	124.0	0.0	C.995	0.000	147	11	7	1.2	:	:	*>
	5 - 6	139.1	1 38.5	0.0	0.996	0.000	154	8	8	0.6	1	3	•>
	6 - 7	156.8	156.2	0.0	0.996	0.000	153	9	10	0.7	:	:	•••••
	7 - E	107.3	166.7	0.0	0.956	0.000	151	12	11	1.2	2		()
	8 - 9	169.7	169.1	0. 0	0.996	0.000	1 41	9	11	1.1	3		4)
	9-10	146.6	146.0	0.0	0.956	0.000	148	7	ę	1.4	:		****
	10 -11	140.4	139.6	0.0	0.996	0.000	145	7	7	1.1	:	:	
	11 -12	133.9	1 33.3	0.0	0.996	0.000	159	9 E	8 8	0.7	: :	•	****
	12-13	137.7	135.3	n. 0	0.963	0.000	145	9	9	1.1	•	•	****>
	13-14	145.4	143.0	0.0 C.0	0.983 C.956	0.000	146 153	11	10	C. 9	:	•	****)
	14-15	139.4	138.8	0.0	0.984	0.000	160	10	10	0.7	:	· ·	*****
	15-16 16-17	149.2	148.6	0.0	0.956	0.000	169	9	9	0.4	•	•	*****)
	1/ -18	163.7	163.1	0.0	0.996	0.000	191	í	12	1.0	1	1	•••••
	18-19	178.5	177.9	0.0	0.997	0.000	191	9	14	0.7	:	- -	>
	17-20	178.2	175.8	0.0	0.987	0.000	199	9	14	1.1	:	:	()
	20 - 51	183.5	162.5	0.0	0.957	0.000	168	7	13	1.0	1	:	* >
	21 - 22	108.7	1 ot . 1	0.0	0.956	0.000	186	6	11	0.7	1	:	*****
	22-23	142.4	141.8	C. 0	0.996	0.000	182	6	8	0.6	:	1	*===>
	23-24	128.9	128.3	U. 0	0.995	0.000	186	6	7	U. 3	:	1	*>
82 OCT 21	0 - 1	124.0	123.4	0.0	C.995	0.000	170	ŧ	7	0.6	:	:	• • • >
02 001 21	1 - 2	117.0	116.4	C. 0	C.935	0.000	161	ŭ	į	0.6	:	1	+>
	2 - 3	111.7	111.1	0.0	0.955	0.000	173	7	6	0.4	:	:	***>
	3 - 4	109.0	108.4	0.0	0.954	0.000	149	7	4	C . 8	1	:	*->
	4 = 5	112.3	111.7	0.0	0.995	0.000	154	7	5	0.7	:	1	+->
	5 - 6	129.1	128.5	0.0	0.995	0.000	155	9	7	0.6	:	:	>
	6 - 7	147.6	147.0	0.0	C.996	0.000	161	7	8	0.6		:	4>
	γ- ε	172.4	170.0	0.0	0.966	0.000	153	7	10	0.5	:	:	A>
	£ - 9	176.1	177.5	0.0	0.997	0.000	177	7	12	0.€	:	•	*>
	→-1 0	166.7	166.1	0. C	C.996	0.000	169	6	1 C	0.4	:	:	*>
	10-11	153.9	153.3	9.0	0.996	0.000	170	e	10	0.5	1	ī	*****
	11-12	153.7	153.1	0.0	C.956	0.000	169	9	9	1.7	:	1	•>
	12-13	146.5	140.0	0.0	0.996	0.000	167	7	ŧ	0.2	:	i	• >
	13-14	148.1	145.7	0.0	0.984	0.000	159	8	7	1.0	:	:	•>
	14-15	141.1	140.5	C. 0	0.956	0.000	158	,	9	0.4	:	•	• • • • >
	15-16	140.2	139.6	0.0	0.956	0.000	163	7	9	0.5	•	:	•>
	16-17	143.5	142.9	0.0	0.996	0.000	183	7	9	0.6	:	:	
	17 - 18	148.5	147.9	0.0	C.996	0.000	181	6	1 C	0.5	:	:	
	16-15	152.3	151.7	0.0	0.996	0.000	185	6	10	0.6	:		*****
	19-20	152.2	151.6	0.0	0.996	0.000 0.000	179 181	7 e	9	0.6 0.8	:	•	*****
	20 - 21	152.0	144.6	0.0	0.984			-	10		:	•	****
	21 - 22 22 - 23	147.F 144.5	147.2	0 . 0 0. 0	0.996	0.000	179 179	8 6	9	1.1	1	•	****
	23-24	110.7	116.1	0.0	0.955	0.000	185	5	΄ έ	0.5	•	•	•>
	63-64	11007	41044	4.4	4.,,,	4 6 0 7 9		•	•	4.7	•	•	- ·

DATE YR PON CY	T I ME S P A N	RIVER FLOW	TURBN FLOW	SPILL FLOW	JUEUN FIVÉR	SPILL HIVEH	DIREC MEAN	T1CN SD	MF W V		31.3	213		1
82 CC 1 22	0 - 1	94.5	93.9	0.0	0.994	0.000	173	8	4	C. E	:	:	(-)	
	1 - 2	12. 3	91.7	0.0	0.753	0.000	169	7	4	0.6	:	:	**>	
	2 - 3	84.8	84.2	0.0	0.953	0.000	163	8	3	0.2	:	:	4->	
	3 - 4	89.9	69.3	C. 0	0.993	0.000	161	7	3	1.0	:	:	•->	
	4 - 5	92.3	91.7	0.0	0.993	0.000	159	5	4	U. 3	:	:	•->	
	5 - 6	105.3	104.7	0.0	C.9>4	0.000	176	6	5	0.7	:	1	•>	
	6 - 7	141-7	141.1	0.0	0.956	0.000	160	5	8	0.3	1	:	****	
	7- 8	152.8	152.2	ი. ა	0.996	0.000	16.5	6	9	U.6	1	1	****)	
	8 - 9	158.3	157.7	C. 0	0.996	0.000	183	6	11	1 • C	:	:	*****	
	9-10	159.€	157.4	0.0	C.985	0.000	168	7	10	0.7	2	:	• >	
	10-11	149.4	146.6	n. v	0.956	0.000	167	6	9	0.7	:	:)	:
	11-12	153.1	152.5	0.0	C.996	0.000	110	8	10	0.7	:	:	*****	•
	12 - 1 2	141. ć	140.6	0.0	0.956	0.000	154	10	ę	0.6	1	:	****>	
	13-14	132.5	131.9	0.0	0.995	0.000	158	8	8	1.0	:	:	*>	
	14 - 15	127.4	126.6	C.C	C.795	0.000	158	11	ę	0.6	:	1	••••	
	15-16	134.2	133.7	0.0	0.956	0.000	160	10	e	0.9	:		• •	
	16-17	131.2	130.6	0.0	C. 955	0.000	162	9	e	1.1	:	•	**** >	
	17 - 18	190.0	18,.4	0.0	C.997	0.000	172	ē	1 4	3.0	:	:	******	
	16-19	153.9	153.3	0. 0	0.956	0.000	174	7	11	0.5	:	•		
	19-20	143.3	140.9	0.0	C.983	0.000	180	5	10	0.5	1	:	*****>	
	20 - 21	123.5	122.9	0.0	0.995	0.000	162	7	9	9.6	1	:		
	21 - 22	118.0	117.4	0.0	C.995	0.000	186	5	7	0.5	1	:	*>	
	22 - 23	106.1	105.5	0.0	0.994	0.000	181	6	6	0.6		:		
	25-24	£3.8	63.2	0.0	0.993	0.000	182	4	4	0.6	1	•	• - >	
82 GCT 23	0 - 1	88.2	87.6	0.0	0.953	0.000	182	6	4	0.6	:	:	* - >	
00 00 . 20	1 - 2	90.5	87.9	0.0	0.953	0.000	178	6	4	0.5	2	:	* ->	
	2- 3	90.1	£9.5	0.0	0.993	0.000	177	6	4	0.6	:	•	•->	
	3 - 4	90.2	87.6	U. 0	C.993	0.000	175	5	4	0.7	1	:	• ->	
	4-5	10.3	£9.7	9.0	0.993	0.000	178	7	5	0.7	:		* ->	
	5-6	90.7	90.1	0.0	0.993	0.000	176	9	5	1.3	1	1	*>	
	6 - 7	93.6	91 . ć	0.0	0.974	0.000	180	7	4	0.6	1	:	*->	
	7 - E	112.5	111.5	0.0	G.955	0.000	185	6	E	0.6	:	:	·>	
	ε - 9	119.8	119.2	0.0	C.995	0.000	180	6	6	0.€	1	:	* >	
	9-1C	135.3	134.7	0.0	C.996	0.000	181	6	9	9.0	1	2	*>	
	10 - 11	138.3	137.7	0.0	0.956	0.000	160	6	9	0.5	:	:	*>	
	11-12	130.6	130.0	0.0	0.995	0.000	179	5	9	0.5	:	1	*>	
	12-13	110.5	109.9	0.0	0.335	0.000	161	5	E	0.6	:	:	•>	
	13-14	99.3	96.9	7.0	0.976	0.000	178	4	6	0.0	:	:	• >	
	14-15	97.6	97.0	0.0	C.954	0.000	186	5	6	0.4	:	:	•>	
	15-16	93.1	92.5	0.0	0.994	0.300	181	6	€	9.6	:	:	**->	:
	16-17	99.1)	9t.4	0.0	0.954	0.000	175	6	6	0.5	:	:	*>	
	17-18	103.1	102.7	0.0	0.956	0.0C0	169	7	5	0.€	:	:	* >	
	16-15	109.2	106.6	1. 0	0.955	0.000	169	5	6	0.4	:	:	4>	
	19-2C	105.9	105.3	C. 0	C.954	0.000	172	10	5	0.7	:	:	* >	
	20 - 21	100.9	100.3	0.0	0.954	0.000	162	4	5	0.6	1	1	•>	
	21 - 22	97.1	90.5	0.0	0.994	0.000	185	5	5	0.6		:	>	
	22 - 23	97. E	97.2	0. 0	0.994	0.COO	160	7	5	0.6	1	:	*>	
	23-24	90.0	89.4	0.0	0.993	0.000	160	6	4	0.2	1		•->	

UATE YR PUN CY	T IME S P A N	RI VER FLOW	TURBN Flor	SPILL FLOW	IUREN Fiver	SEILL RIVER	DIREC MEAN		MEAR		31 3	213	1
82 OCT 24	0 - 1	94.8	22.4	0.0	0.975	0.000	155	7	5	0.0	:	:	·->
	1 - E	8 3. 1	82.5	0.0	0.953	0 - 0 00	130	7	3	0.5	3	1	* - >
	2 - 3	81.6	81.0	0. 0	0.953	0.000	136	9	3	0.7	I	1	•>
	5- 4	85.1	80.7	0.0	0.9/1	0 . 0 1 0	144	8	3	0.6	1	1	•>
	4 - 5	61.6	61.0	0.0	0.993	0.0(1)	139	4	2	U.6	2	:	•>
	5-6	82.7	82.1	0. 0	C.993	0.000	145	6	2	0.5	1	1	•>
	6 - 7	86.2	83.6	0.0	0.972	0.000	143	5	4	0.5	2		4->
	7 - 8	83.6	83.0	0.0	0.993	0.000	144	6	3	1.0		ŧ	•>
	B - 9	86.4	85.8	C. 0	0.993	0.000	139	4	4	0.3	:	:	• ->
	9-10	103.7	103.1	0.0	0.954	0.000	149	6	5	0.6	1	•	4->
	10-11	104.4	102.0	0.0	0.977	0.000	146	8	4	0.5	•	1	• -> :
	11 - 12 12 - 13	101.3 99.2	101.2 96.6	c.o n.o	0.994	0.000 0.000	147	8	i	0.6	:	:	4-> 1
	15-14	97.5	96.9	0. 0	0.954	0.000	149	10	,	0.7	:	•	•••
	14-15	96.1	95.5	0.0	0.954	0.000	145	7	ž	0.4	1	:	4.
	15-16	93.8	91.4	0.0	0.974	0.000	145	6	- 1	0.6	:	•	• • >
	16-17	89.4	88.9	0.0	0.954	0.000	142	6	•	1.0	:	;	•-> •>
	17 -18	92.9	92.3	0.0	0.954	0.000	1 47	,		0.7	:	•	•->
	16 - 19	104.9	104.3	0.0	0.554	0.000	146	5	5	0.3	:	;	4->
	17-20	105.2	104.6	0.0	0.994	0.000	147	á	é	1.1	1	•	4***)
	20 - 21	103.7	103.1	0.0	0.954	0.000	149	,	7	U. 9	i	•	****
	21 - 22	103.0	103.2	0.0	0.994	0.000	176	10	5	1.1	:	•	* - >
	22 - 23	105.9	103.5	0.0	0.977	0.000	174	6	Ś	0.4	:	ī	+->
	25-24	93.6	93.0	0.0	0.994	0.000	152	5	ž	0.6	1		•>
_								_	-	•••	-	•	• •
82 CCT 25	0 - 1	85.0	82.6	c. o	0.972	0.000	1 4 3	10	3	1.C		:	*->
	1 - 5	63.0	62.4	0.0	0.953	C.000	150	6	3	0.5	•	•	1->
	2 - 3	84.1	83.5	0.0	0.993	0.000	1 3 5	8	3	3.0	:	1	• •
	3 - 4	85.5	84.9	0.0	C.953	0.000	138	7	4	0.5		•	••>
	4 - 5 5 - 6	91.6 90.9	69.4 90.3	0.0	0.974	0.000	138	7	4	1.0	:	•	4->
	6-7	118.4	117.8	0.0	0.993	0.000 0.000	135 155	9	3	0.7	1	•	4->
	7 - 8	140.0	139.4	0.0 0.0	0.996	0.000	170	9 10	7	0.6	1 1	•	***>
	8- 9	143.1	142.5	0. 0	0.996	0.000	164	8	10 10	0.8	:	•	4===>
	9 - 1 C	119.0	115.2	0.0	C.955	0.000	157	9		1.2	:	•	****
	10-11	116.0	117.4	0.0	0.955	0.000	158	10	7	3.0	:	•	*>
	11-12	118.2	115.8	0. 0	C. 980	0.000	169	iĭ	į	0.9	:	•	***>
	12-13	116.2	117.€	0.0	0.995	0.000	164	ç	Ė	0.6		-	***>
	13-14	102.9	102.3	0.0	0.994	0.000	154	É	5	0.7			***
	14-15	101.6	100.9	0.0	0.953	0.000	155	9	é	0.7		•	***>
	15-1€		•			• • • • • • • • • • • • • • • • • • • •	169	12	-	1.4	2	•	40000
	16-17	118.6	110.0	0.0	0.995	0.000	182	iż		i.c	:	-	******
	17 -18	122.3	121.7	0.0	0.755	0.000	194	11		1.0	2	•	
	18-15	132.8	132.2	0.0	0.955	0.000	196	11		1.0	1	:	4>
	17-20	154.8	134.2	C. 0	C.956	0.000	187	e		1.3	:	:	******
	20 - 21	132.8	132.2	0.0	0.955	0.000	186	10	15	1.2	:	2	*****
	21 - 52	131.7	131.1	v. n	0.955	0.000	167	6	11	0.5	:	:	****
	22 - 23	107.8	107.2	0. 0	0.994	0.000	173	10	9	1.0	1	:	4> ·
	23-24	101.3	100.7	0.0	0.954	0.000	148	12	11	1.2		1	>

DATE YR PUN DY	T IME SPAN	RI VER FLUH	TURBN FLOW	SPILL FLUH	IU3EN KIVER	SPILL	DIREC MEAN	TION SD	VELC. MÉAR		31 3	213	11
82 CCT 26	0 - 1	100.7	100.1	0.0	C.954	0.000	143	12	1 C	1.3	:	: ***	> :
	1 - 2	99.6	99.0	0.0	0.954	0.000	155	10	7	0.9		: •>	•
	2- 3	91.2	90.6	0.0	0.953	0.000	151	9	4	0.7	:	: +->	
	5 - 4	89.4	88.6	0.0	C.993	0.000	164	٩	5	0 . F	:	: ••>	:
	4- 5	£ 9.0	8t.4	0.0	0.993	0.000	178	۲	6	0.4	:	1 +>	:
	5 - 6	105.4	104.8	0.0	0.954	0.000	176	12	6	0.E	1	: +>	:
	6 - 7						164	10	9	0.7	:	; ,>	:
	7 - E	184.4	162.0	0.0	0.967	0.000	170	5	11	0.9	:	‡ *****>	:
	8- 9	186.0	183.6	C. C	0.967	0.000	167	7	11	1.2	:	: (******)	:
	9-10	156.1	155.5	0.0	0.956	0.000	1 2 4	11	9	0.9	•	:	•
	10-11	148.7	148.1	0.0	0.996	0.000	167	11	9	1.3	:	: •>	:
	11-12 12-13	135.7	135.1	0.0	0.796	0.000	159	14	7	1-7	:	: +> : +>	:
	15-15	155.8 159.7	155.2 159.1	0. 0 C. 0	0.956 0.956	0.000	161 157	10 11	10 10	1.0	•		:
	14-15	147.9	147.5	0.0	0.956	0.000	151	16	9	2.1	• •	1 4	
	1>-16	137.6	137.0	0.0	0.956	0.000	159	12	9	1.0	:		•
	16 - 17	160.7	160.3	C. C	0.936	0.000	154	9	11	1.6	•		
	17 - 18	150.9	150.3	0.0	0.956	0.000	169	7	10	1.2	-		•
	18-19	149.9	149.3	0. 0	0.956	0.000	159	8	9	0.9	•	: •>	
	19-20	146.2	145.6	0. C	0.996	0.000	152	10	ģ	0.7	:		:
	20-21	136.3	133.9	0.0	0.982	0.000	161	12	ė	1.7	:	; +>	:
	21 - 22	128.7	126.1	0.0	0.935	0.000	172	7	7	0.7	:	: ••••>	:
	22 - 2 3	124.C	123.4	0.0	0.955	0.000	173	7	7	0.6		: +>	:
	23-24	105.7	105.1	4. 0	0.994	0.000	175	5	6	3.0	•	ŧ +>	1
82 CCT 27	0 - 1	105.2	104.6	C. 0	C.954	0.000	179	5	6	0.5	2	: •=->	
02 (0) 21	1 - 2	104.4	102.0	0.0	0.917	0.000	175	ź	ì	0.7	1	: •-=>	;
	2 - 3	102.0	101.4	0.0	0.994	0.000	179	ė	7	0.6	<u>.</u>	t +>	:
	3 - 4	102.3	101.7	0.0	C.934	0.000	179	8	6	0.6	:	1 +>	;
	4- 5	102.7	102.1	0.0	0.954	0.000	187	7	6	0.7	:	; •>	:
	5 - 6	103.9	103.3	0. 0	0.954	0.000	184	7	6	0.6	:	; •>	:
	6 - 7	133.4	132.8	0.0	0.956	0.000	185	7	E	0.5		: •>	:
	7 - 8	190.7	190.1	7.0	9.957	0.000	185	7	1 4	U.7	:	: 4*****>	:
	8- 6	186.2	185.6	C. 0	C.957	0.000	187	6	13	0.6	:	* ******	:
	9 - 1 C	156.9	154.5	0.0	0.965	0.000	191	5	9	0.6	:	{	:
	10-11	149.5	146.9	0.0	0.996	0.000	185	6	9	0.6	:	1 4>	:
	11-12	156.4	155.6	C. C	C.956	0.000	184	4	9	0.4	:	; •>	:
	12-13	160.€	160.2	7.0	0.996	0.000	176	7	10	1.0	:	?	:
	13-14	161.7	159.5	0. 0	0.985	0.000	177	6	1 C	0.6	:	: ••••>	:
	14 - 15	157.1	156.7	0.0	C.985	0.000	171	. 5	11	1.0	:	•>	:
	15-16	154.0	153.4	0.0	0.956	0.000	165	11	11	1.5	:	• • • • • • • • • • • • • • • • • • • •	:
	16-17	157.7	155.3	0.0	0.985	0.000	164	8	1 C	0.9	:	; #>	:
	17 -18	160.3	156.9	0.0	0.951	0.000	156	10	15	1.0	:	* ******	
	10 - 19 19 - 20	155.6 156.0	155.0 153.6	0.0	0.996 C.985	0.000 0.000	165 163	9 5	1 C 9	0.7	:	; +>	:
	20-21	152.7	150.3	0.0 0.0	0.964	0.000	173	7	9	0.5	:	• • • • • • • • • • • • • • • • • • • •	:
	21 - 22	143.4	142.8	0.0	0.996	0.000	170	6	ě	0.6	:	: •>	:
	22-23	128.)	128.3	0.0	C.955	0.000	180	8	7	0.7	:	: •••>	:
	23 - 24	125.7	123.3	9.0	0.961	0.000	171	9	'n	0.7		: •>	:
		16701	• • • • •	4. 4	U . 7 C L	.,		,	•	V • 1	•	, , , , , , , , , , , , , , , , , , , ,	•

DATE YR PUN CY	TIME	RIVER FLOR	TURBN FLOW	SPILL , FLU W	INEBN	PIVEH	DIREC MEAN	TION	VEL CO ME A A		31 3	213	1	1
82 OCT 28	0 - 1	121.0	120.4	0.0	0.995	0.000	173	7	7	0.4	:	: ••	••>	:
02 20 7 20	1 - 2	117.6	117.0	0.0	0.955	0.000	179	5	6	0.6	:	1 +:	•	:
	2 - 3	116.	116.3	0.0	0.955	0.000	181	5	E	0.4	:	: +:		:
	3 - 4	116.6	116.C	0.0	0.945	0.000	172	6	E	0.5	:	: ••		:
	4 - 5	119.8	117.4	0.0	0.960	0.000	171	7	7	0.0	1	:		:
	5 - €	120.2	119.6	0.0	C.995	0.000	180	5	6	0.4		1 4		:
	6 - 7	152.3	149.9	0.0	0.964	0.000	166	6	9	0.5	:	1		:
	7 - ε	166.2	187.6	c.o	0.957	0.000	178	10	14	1.7	:	: *		:
	8 - 5	182.2	181.6	0.0	0.957	0.000	180	8	1.3	0.4	:	: •		:
	9-10	173.6	173.0	0.0	0.957	0.000	177	10	13	0.5	:	: •		:
	10-11	168.1	167.5	1). ()	0.996	0.000	178	e	1 3	1 - 1	:	: •••		:
	11-12	167.4	166.8	C. O	0.996	0.000	116	ð	12	0.6	:	: •••		:
	12-13	166.8	166.2	n. 0	0.996	0.000	176	٤	13	0.4	:	1 4		:
	15-14	171.6	169.2	0.0	0.966	0.000	176	8	1 3	1 . C	:	: •		3
	14-15	105.6	165.0	C. 0	C.996	0.000	168	7	11	0.4	:	-		1
	15-16	171.7	171.1	0.0	n.957	0.000	182	٩	13	v. 5	:	•		:
	16-17	174.7	174.1	0.0	0.997	0.000	178	8	1 3	C.7	1	•		1
	17 -18	178.8	176.2	0.0	0.957	0.000	182	9	15	0.7	:			:
	1t -19	100.4	179.6	0.0	0.997	0.000	178	9	15	0.t	:	•		:
	13-50	179.9	179.5	C. 0	0.957	0.000	184	7	13	0.7	:	•	•	:
	20 - 21	169.8	169.2	.n. n	0.956	0.000	162	٩	13	0.7	1	•	•	:
	21 - 22	156.8	156.2	9.0	0.996	0.000	180	7	12	0.7	:	•	•	:
	22 - 23	148.)	148.3	0.0	C.956	0.000	177	ð	9	0.7	:	•	•	:
	23-24	126.5	125.9	0.0	0.995	0.000	170	9	9	1.1	:	1	>	:
								_	_				>	
FS OC 1 59	0 - 1	112.4	111.8	0.0	0.995	0.000	167	7	9	1.C		:		1
	1 - 2	110.6	110.0	C. 0	C.995	0.000	170	7	e	0.7	:	•		1
	2 - 3	112.2	109.6	n. 0	0.979	0.000	177	6	6	0.3	:	• • • • • • • • • • • • • • • • • • •		:
	3 - 4	110.3	109.7	0. 0	0.955	0.000	177	7	6	0.4	:	: • • • • • • • • • • • • • • • • • • •		:
	4 - 5	112.2	111.6	0.0	0.995	0.000	174	7	•	0.3	1			:
	5 - 6	112.6	112.0	n. 0	0.995	0.000	167	6	6	0.5	:	:		:
	6 - 7	146.0	145.4	C. 0	0.956	0.000	165	7		0.6	:	:		
	7 - E	166.2	187.6	0.0	0.957	0.000	1/6	٤	1 4	0 · Ł	:			:
	b - 9	194.0	193.4	C. 0	0.997	0.000	180	9	15	0.7	•			:
	9 • 1 C	18C.3	179.7	C. 0	0.957	0.000	180	7	14	3.0	:			:
	10-11	169.8	169.2	0.0	0.956	0.000	161	e	13	1.0	:	; •	-	:
	1: -12	173.7	173.1	0.0	C.957	0.000	175	8	12	9.0	:	•		:
	12-13	164.7	164.1	0.0	C.996	0.070	177	6	11	0.6	:			:
	13-14	171.1	170.5	0.0	0.996	0.000	167	10	12	0.8		· · · · · · · · · · · · · · · · · · ·	••••>	•
	14-15	167.4	166.0	0.0	0.956	0.000	172	8	11	3.0	:	-	•	:
	15-16	167.1	166.5	0.0	0.956	0.000	171	9 8	10	0.5	:	•	•	:
	10-17	177.5	176.9	0.0	0.997	0.000	163		1 C 1 5	1.0	:	•		:
	17 - 18	198.9	198.3	C. 0	C.997	0.000	169 159	11 13	14	0.7	•	•		:
	18 = 19	214.5	213.9	0.0	0.997 C.957	0.000	163	12	15	1.6	:	•	-	:
	17-20	216.4	215.8	C. 0	0.957	0.000	165	10	14	1.0	•	•	- ·	:
	20 - 21	207.6	205.2	0.0	0.966	0.000	153	8	12	1.5	•	•	=	:
	21 - 22 22 - 23	197.3	190.7	0.0 0.0	0.956	0.000	162	10	7.5	1.2	:	;		:
	23 - 24	139.9	139.3	0.0	0.936	0.000	153	12	7	0.6	:	• •		
	23-24	43707	A 370 3	414	., . , , ,	240.00	• • • •	• -	•	3.0	٠	-		

DATE YR MON DY	TIME	RI VER FLOW	TURBN Flow	SPILL FLUW	HINER	SPILL FIVER	DIRECTION MEAN SD		CITY	31 3	213	11
82 CCT 30	0 - 1	131.7	1 31.1	0.0	0.955	0.000	149 10	7	1.1	:	:	·> :
	1 - 2	135.4	1 33.0	0.0	0.465	0.000	148 13	7	0.8	:	:	•> :
	2 - 3	152.3	1 32.2	0.0	C. 995	0.000	139 10	6	0.5	:	:	*> :
	3 - 4	154.4	1 33.6	C. 0	C.996	0.000	143 7	7	9.0	:	:	•> ;
	4 - 5	140.1	1 39.5	ი. ს	0.956	0.000	157 9	8	U.7	:	1	> :
	5 - 6	146.3	1 45.7	0. 0	0.956	0.000	152 10	7	1.1	:	\$	·> :
	6 - 1	166.8	1 66.2	0.0	0.956	0.000	156 13	9	0.E	:	••	·•> ;
	7 - 8		176.6	u. 0	0.967	0.000	157 14	12	1.2	:	1	> :
	e - 9	185.2	184.6	0.0	0.957	0.000	157 11	11	1.5	1	••	> :
	9-10	199.3	191.7	0.0	0.057	0.000	150 11	1 6	4.2	2	.	:
	10-11	201.5	200.9	7.0	0.997	0.000	155 9	12	1.0	:	: •-	> ;
	11 - 12	195.5	193.1	0.0	939.0	0.000	152 13	1 3	1.3	1	:	· :
	12-13	182.9	180.5	0.0	0.967	0.000	149 €	10	1.2	:	:	4>
	13-14	170.8	170.2	0.0	0.956	0.000	151 9	10	1.8	1	:	•>
	14 - 15		15C.7	c. o	0.356	0.000	146 8	8	0.3	:	1	*> ;
	15-16	146.5	1 45.5	0.0	0.956	0.000	150 11	ę	1.2	1	:	*> :
	16-17	156.2	153.6	0.0	0.985	0.000	146 10	9	1.C	•	.	4> ;
	1/ -18	17 4. 1	173.5	0.0	0.957	0.000	151 9	11	1.3		:	•> :
	16-19	188.3	167.7	0.0	0.997	0.000	161 9	13	1.7	•	i +•·	> :
	19 - 20	_	1 87.9	0.0	0.997	C.000	151 10	12	1.2	:	:	4> :
	20 - 21	166.4	165.6	0.0	0.997	0.000	152 12	11	1.6	:	;	•> :
	21 - 22	172.2	171.6	0.0	0.997	0.000	153 15	1 1	1.1	:		•> :
	22.51	158.8	156.4	C. 0	0.985	0.000	155 9	8	0.6	:	-	>
	23-24	148.5	147.9	0.0	0.996	0.000	153 9	e	1.3	:	*	•> :
82 OCT 31	0 - 1	141.0	1 40.4	0.0	C.996	0.000	146 12	7	1.4	*	:	·> :
	1 - 2	140.3	1 39.7	D. 0	0.956	0.000	144 12	7	1.6	1	3	*> :
	2 - 3	139.7	1 37.1	ŋ . ŋ	0.996	0.000	149 13	7	1.0		:	•>
	3 - 4	139.5	1 30.9	C. O	C.996	0.000	153 11	7	1.3	1	:	•> :
	4 - 5	143.5	142.5	0.0	0.956	0.000	156 10	7	0.9	1	: ••	> :
	5 - 6	146.5	1 47.9	0.0	0.956	0.00	156 10	7	1.0	1	: ••	> :
	6 - 7	151.7	151.1	c. o	C-916	0.000	161 9	8	0.6	1	: •=•	> :
	7 = E	179.2	176.t	າ. 0	0.967	0.000	157 9	ŧ	1.9	1	: ••	> :
	6 - 9	166.1	187.5	0.0	0.557	0.000	161 8	1 C	1.0	:	:	> :
	9 - 1 C	216. P	214.4	C. 0	0.983	0.000	152 9	12	1.2	:	.	•••••
	10 - 11	217.5	215.1	0.0	0.989	0.000	160 14	15	1.4	:	\$ **·	> :
	11-12	203.5	202.9	0.0	0.957	0.000	161 14	16	1.2	:	:	> ;
	12-13	190.9	180.5	0.0	C. 987	0.000	161 13	15	1.2	1	:	> :
	15-14	166.8	164.4	0.0	0.925	0.000	160 12	12	1.7	:	: +	> :
	14-15	145.2	144.6	0.0	0.956	0.000	160 13	9	1.9	:	:	> :
	15 - 16	143.2	142.6	0.0	0.956	0.000	164 10	ē	1.1	1	:	·> :
	16-17	154.3	151.9	1. 1	0.984	0.000	168 10	9	1.4	:	:	•> 1
	17 -18	169.5	160.7	0.0	0.796	0.000	162 10	9	1 . 4	:	<u>-</u>	> :
	16-15	176.3	175.7	0. n	0.057	0.000	164 11	12	0.9	:	:	·> :
	19-20	165.5	154.9	0. U	0.256	ი. ია	168 9	11	1.3	:	: +	·> :
	20 - 21	161.6	161.0	0. C	0.756	0.000	171 8	11	9.0	:	: 4	-
	21 - 22	157.8	157.2	U. 0	0.756	0.000	169 11	9	1 • 1	:	: +;	-
	22 - 23	141.5	140.9	0. 0	C. 956	0.000	174 7	11	0.9	ı	: +	•
	23-24	128.7	120.1	0.0	0.955	0.000	162 13	7	0.5	:	* * * * * * * * * * * * * * * * * * *	> 1

82 ADY 1 0-1 111-0 111-0 0.0 0.0 0.095 0.000 147 11 7 0.99 1 1	DATE YR PON CY	T IME Spak	RIVER FLOW	TURBN FLOW	SPILL FLOW	TUPEN RIVER	SPILL HIVER	DIREC MEAN	T L D N S D	MEAR		313	213		1.1
1 - 2 105.7 103.5 0.0 0.027 0.000 143 16 5 0.5 1 1	82 NOV 1	0 - 1	111.6	111.0	0.0	0.955	0.000	167	11	7	0.9	1	1	•>	:
3 - 1 106.7 106.3 0.0 0.474 10.00 151 11 6 0.6 2 1 1 1 4 - 5 111.5 112.9 0.0 0.755 1.000 157 17 6 1.2 1 1		1 - 2	105.9	103.5	0.0	0.977	0.000	145	16	5	0.5	2	1	•->	:
## 4 : \$ 111.5 112.9 0.0 0.955 0.000 157 12 6 1.2 1 1 1 1 1 1 1 1 1		2 - 1	106.	105.7	C. O	0.994	0.000	142	9	4	1 - 1		1	• - >	:
3 - 6		5 - 4	106.9	1 C b • 3	0.0	0.954	0.000	151	11	6	C • 8	:	1	+>	፡
6 7 164.1 161.5 0 0.0 0.957 0.000 152 7 8 6 1.1 1 1 2		4 - 5	113.5	112.9	0.0	0.995	6.000	157	12	6	1.2	:	:	•>	:
		5-6	136.1	135.5	0.0	C.956	0.000	155	11	5	1.0	:	3	*~->	:
1		6 - 7	164.1	165.5	a. n	0.956	0.000	15?		E		1	3	•>	-
19-10 15-16 15-16 15-16 0.0 0.356 0.000 15-12 5 1.6 1 1 11-12 15-13 15-17 0.0 0.356 0.000 15-10 15-13 15-12 1 11-12 14-13 14-15 14		7 - E	163.4	162.6	0.0	0.997	0.000	154		10	0.7	:	:	•>	
19-11 197,3 156,7 0.0 0.796 0.000 194 12 6 1.2 1 1.2		8- 5	159.7	159.1	0.0	0.946	0.000	147	10	17	1.4	:	:	•>	:
11-12		9-1C	151.€	151.0	0.0	1. 956	0.000	144	12	ç		1	1	·>	:
12-11 11/1.5 116.7 0.0 0.995 0.000 14.9 8 1.2 1 1 1 1 1 1 1 1 1		10-11	157.3	156.7	0.0	0.996	0.000	154	12	8	1.2	:	:	•>	:
11		11-12	143.9	143.2	C. 0	0.196	0.000	158	•	e	1 • C	:	:	* >	-
10-15 131,7 135,1 1.0,0 0.966 0.000 149 8 6 1.1 1 1.5 1.5 1.5 1.42,0 0.0,0 0.966 0.000 160 9 9 0.9 1 1 1.5		12-13						152	11	6	1.5	:	:	* >	
12-16 142.6 142.0 0.0 0.966 0.000 162 9 10 0.7 1 1 1.0 161.5 1.0 0.0 0.967 0.000 165 9 9 0.9 1 1 1.0		13-14	117.5	116.7	0.0	C. 955	0.000	154	10	8	1.2	:	1	*>	:
16-17		14-15	133.7	133.1	C. 0	C•936	0.000	149	8	6	1.1	:	:	4>	:
17-16		15-16	142.6		0.0			162	٩	-		1	:	*>	:
18-15 220.8 218.4 0.0 0.949 0.000 166 11 17 2.1		16-17	184.5	183.9	0.0	C.997	0.000	166	9		0.9	1	1	•>	:
19-20 212.3 209.9 0.0 0.989 0.000 181 10 20 3.3 1 2 2 2 2 2 2 2 2 2		17-18	214.6	214.C	0.0	0.937	0.000	170	9	1.5	0.5	:	:	>	:
20-21 25,7 20.3 0.0 0.957 0.000 190 12 20 3.1 1 1 1 1 1 1 1 1 1		18-19	220.8	218.4	0.0	0.969	0.000	166	11	17	2.1	:	1	******	:
21-22 194.1 191.7 0.0 0.956 0.000 194 17 2C 3.6 : : :		19-20	21 2. 3	209.9	0.0	C.989	0.000	181	10	20	3.3	:	:	4>	:
1		20-21	205. 7	205.3	0.0	0.957	0.000	190	12	20	3.3	1	1		:
EZ NUV 2 0-1 143.8 143.2 0.0 0.956 0.000 185 7 12 0.9 : :> : 1- 2 138.0 137.4 0.0 0.956 0.000 187 6 9 0.9 : :> : 2- 3 130.4 128.0 0.0 0.956 0.000 187 6 9 0.9 : :> : 2- 3 130.4 128.0 0.0 0.000 184 5 7 0.6 : :> : 3- 4 150.2 149.6 0.0 0.956 0.000 184 5 7 0.6 : :> : 4- 5 159.7 159.1 0.0 0.956 0.000 184 5 7 0.6 : :> : 5- 6 182.0 181.4 0.0 0.957 0.000 182 6 10 1.2 : :> : 6- 7 204.2 203.6 0.0 0.957 0.000 180 7 11 0.6 : :> : 7- 6 246.5 245.5 0.0 0.957 0.000 180 7 11 0.6 : :> : 8- 9 149.9 199.3 0.0 0.957 0.000 184 11 20 3.2 : :> : 10-11 175.5 175.0 0.0 0.957 0.000 181 11 12 10 : :> : 11-12 191.1 190.5 0.0 0.957 0.000 184 11 20 3.2 : :> : 12-13 186.8 187.0 0.0 0.957 0.000 177 8 12 1.0 :> : 12-13 186.8 187.0 0.0 0.957 0.000 187 18 18 18 18 18 18 18 18 18 18 18 18 18		21-62	194.1	191.7	0.0	9.968	0.000	194	17	2 C	3.€	:	2	>	:
62 NUV 2 0-1 143.8 143.2 0.0 0.996 0.000 182 6 1C 0.5 : :		22 - 23	168.4	167.8	C. 0	C.996	0.000	193	10	16	0.E	2	:		;
1 - 2		23-24	153.f	153.2	0.0	0.956	0.000	185	7	12	0.9	:	1	>	:
1 - 2	62 NUV 2	0 - 1	143.8	143.2	0. 0	0.946	0.000	182	6	1.0	0.5	•	•	••••>	:
2- 3 150.4 12t.U 0.0 C.9t2 3.000 184 6 9 0.6 : : **> : 3- 4 150.2 149.6 0.0 C.956 0.000 184 5 7 0.6 : : **> : 4- 5 159.7 159.1 C.0 0.956 0.000 182 6 10 1.2 : : **> : 5 16 182.U 181.4 0.0 0.957 0.000 178 6 10 0.7 : : **> : 5 16 182.U 181.4 0.0 0.957 0.000 178 6 10 0.7 : : **> : 5 16 182.U 181.4 0.0 0.957 0.000 180 7 11 0.6 : : **> : 5 17 - 6 246.5 245.5 0.0 0.957 0.000 180 7 11 0.6 : : **> : 5 18 - 9 179.9 179.3 0.0 0.957 0.000 184 11 20 3.2 : : **> : 5 11 1 1 179.5 0.0 0.957 0.000 184 11 20 3.2 : : **> : 5 11 1 1 179.5 0.0 0.957 0.000 184 11 20 3.2 : : **> : 5 11 1 1 179.5 0.0 0.957 0.000 184 11 20 3.2 : : **> : 5 11 1 1 1 179.5 0.0 0.957 0.000 177 8 12 0.0 : **> : 5 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.5 1104 5					-		-				=	-	• • • • • • • • • • • • • • • • • • •	
3-4 150.2 149.6 0.0 0.956 0.000 184 5 7 0.66 : : :		-						-				1	•	+ >	:
4-5 159,7 159,1				-		-			-			-	1	>	
5-6 182.0 181.4 0.0 0.997 0.000 178 6 1C 0.7 ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;				_				-		-		1	1	****>	:
6-7 204.2 2C3.6 0.0 C.957 0.000 180 7 11 0.6 : :> : 7- 6 246.5 245.5 0.0 0.957 0.000 177 7 15 1.1 : :> : 8- 9 1/9.7 199.3 0.0 0.957 0.000 184 11 20 3.2 : :> : 9-1C 180.1 175.5 175.0 0.0 0.997 0.000 181 10 16 1.0 : :> : 10-11 175.5 175.0 0.0 0.997 0.000 181 10 16 1.0 : :> : 11-12 1/1.1 190.5 0.0 0.997 0.000 177 8 12 1.0 : :> : 12-13 168.6 188.2 0.0 0.997 0.000 172 8 12 C.5 : :> : 12-14 163.6 185.0 0.0 0.997 0.000 172 11 15 0.6 : :> : 14-15 183.5 181.7 0.0 0.997 0.000 185 10 16 1.1 : :> : 15-16 208.4 207.6 0.0 0.997 0.000 185 10 16 1.1 : :> : 17-18 214.6 214.6 0.0 0.997 0.000 191 10 19 1.5 :> : 17-18 214.6 214.6 0.0 0.997 0.000 191 11 16 5.2 :> : 18-15 231.1 230.5 0.0 0.997 0.000 176 10 18 4.0 :> : 18-15 231.1 230.5 0.0 0.997 0.000 176 10 18 4.0 :> : 19-2C 253.8 251.4 0.0 0.997 0.000 176 10 19 3.5 :> : 21-22 219.5 219.0 0.0 0.997 0.000 179 12 2C 0.5 :> : 22-21 197.0 196.4 C.0 C.997 0.000 179 12 2C 0.5 :> :												1		*****	
7 - 6			-						-				· ·	******	
8-9 179.7 199.3 0.0 0.957 0.000 184 11 20 3.2 : : *********************************												•	•		
9-1C 180.1 179.5 0.0 0.997 0.000 161 10 16 1.0 : : :												:	·	******	:
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14-15			_										•	******	:
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17 - 18								-				•	•		
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20-21 236.0 235.4 0.0 0.957 0.000 180 9 21 3.2 8 : ********** : *********************												-	<u>.</u>	<u></u>	:
21-22 219.5 219.0 0.0 0.997 0.000 182 11 21 0.8 1 : *> : 22-23 197.0 196.4 C.O C.997 0.000 179 12 2C 0.5 1 : *> :		_								_		-	•	*******	:
22-23 197.0 196.4 C.O C.957 0.000 179 12 2C 0.5 1 :					-	-						•	• •	.)	:
LL L1 1/100 1/004 000 00/// 00000 11/ 11/ 00 000					-							•	•		
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DATE YR PUN CY	TIME	RI VEH FLOW	TURBN FLOW	SPILL FLOW	IUBZN Fiver	SPILL	DIRECTION SD		CITY	31 3		213		1
82 NOV 3	0 - 1	177.1	174.7	0.0	0.986	0.000	183 10	15	0.5	:		:	* >	•
0000	i - č	140.6	140.0	0.0	0.956	0.000	179 9		0.6	:		1	·>	:
	2 - 3	132.3	131.7	0.0	0.995	0.000	180 6	9	0.€	1		3	•>	•
	3 - 4	133.8	135.2	0.0	0.996	0.000	176 5	: e	0.5	:		2	• >	-
	4 - 5	139.7	139.1	C. 0	0.996	0.000	175 6	, 7	0.5	•			• >	
	5 - 6	171.3	171.2	0.0	0.957	0.000	170 6	7	0.4	:		:	****>	:
	6- 7	196.1	193.7	0.0	932.0	0.000	177 7		0.5	•		•	*>	:
	7 - E	208.3	207.7	0.0	0.957	0.000	169 6		0.5	•		:	**>	1
	8 - 9	17 3.5	172.9	0.0	C.997	0.000	172 10		C . e	:		:	4>	:
	3-10	168.4	167.6	0.0	0.936	0.000	161 5		0.4	•		:	******	:
	10-11	149.1	148.6	0.0	0.957	0.000	178 8		0.€	I		•	>	•
	11-12	167.6	167.C	0.0	0.956	0.000	177		0.7	:		•	*>	:
	15-13	163.5	162.9	1). ()	0.996	0.000	163 76		0.0	•	_	•	•	
	15-14	160.9	160.3	0.0	0.996	0.000	288 1	. 0	0 • C	i	•	:		•
	14-15	162.6	160.5	0.0	0.985	0.000				2		•		:
	15-16	161.0	160.4	0.0	0.996	0.000				•		:		•
	16 - 17	169.0	168.4 201.2	C. C	0.956 0.957	0.000				1		•		•
	17 - 18	201. P 197. 5	178.9	0. 0	0.977	0.000				3		3		·
	18 - 19 19 - 20	187.4	185.0	0.0	0.987	0.000				:				:
	20 - 21	157.7	157.1	n. u	0.996	0.000				1		•		:
	21 - 22	153.7	151.3	0. 0	0.964	0.000				:		•		
	22 - 2 3	130.7	128.3	0.0	0.982					:		1		•
	23 - 24	128.3	125.9	0.0	0.981	0.000				:		1		•
	23 6 7	12000		,,,	•••••									
82 NOV 4	J-1	11 0. 0	109.4	C. 0	0.995	0.000						•		
	1 - 2	105.6	105.2	0.0	0.954	0.000				:		:		
	2 - 3	95.7	90.1	0.0	C.994	0.000				:		i		
	5 - 4	67.9	61.3	0.0	0.993	0.000				3		:		
	4- 5	95.0	92.6	ე. 0	0.915	0.000				1		1		•
	5 - 6	120.9	120.3	C. O	0.955	0.000				1		3		
	6 - 7	148.7	148.1	c. o	C.996	0.000				•				:
	7- E	176.9	176.3	0.0	0.957	0.000				i		•		-
	8 - 9	171.2	170.6	0.0	C.996	0.000				Z		:		:
	9-10	158.3	157.7	n. n	0.956	0.000				.		•		:
	10-11	157.5	156.9	0.0	0.996	0.000				:		:		•
	11-12	150.7	150.1	0.0	0.996	0.000				•		•		•
	12-13	156.7 149.2	156.1 148.6	0.0	0.996 C.996	0.000				:		:		:
	13-14	157.3	156.7	0. 0 0. 0	0.996	0.000				•		:		
	14 - 15 15 - 16	157.2	156.6	0.0	0.956	0.000						:		·
	16-17	165.0	162.6	0. 0	0.985	0.000				1		:		:
	17-16	200.6	200.0	0.0	0.957	0.000				I .		:		1
	16-19	208.5	207.9	0.0	0.997	0.000				-		•		•
	19-20	199.3	178.7	C. 0	C.997	0.000				•		•		:
	20-21	192.1	185.7	0.0	0.986	0.000				:		1		:
	21 - 22	174.3	173.7	0.0	0.957	0.000								•
	22 - 23	149.5	148.9	C. 0	0.996	0.000				•		:		:
			131.9											